## CivTech

August 30, 2022
Mr. Christopher Brown, FASLA, LEED AP, SITES AP Floor Associates
1425 North $1^{\text {st }}$ Street, Suite 200


Expires 12/31/2023

Phoenix, Arizona 85004

## Re: Traffic Impact Statement for a Park with Pickleball and Basketball Courts, Ashler Hills Drive at 74 ${ }^{\text {H. }}$ Way - Phoenix, Scottsdale

Dear Mr. Brown:
Thank you for retaining CivTech to provide a traffic impact statement (TIS) for Floor Associates (the "Client") for the park development, consisting of pickleball courts, a basketball court, picnic ramadas, and trails with 70 parking spaces located at Ashler Hills Drive at $74^{\text {th }}$ Way in the City of Scottsdale, Arizona. There will be one (1) proposed site access at the roundabout at $74^{\text {th }}$ Way and Ashler Hills Drive. A vicinity map of the site is shown in Figure 1. This statement is in response to the City of Scottsdale's $1^{\text {st }}$ Submittal comments. Comments and responses are provided in Attachment A. An attachment of the site plan is provided in Attachment $\mathbf{B}$.


Figure 1 - Vicinity Map

CivTech Inc. • 10605 North Hayden Road • Suite 140 • Scottsdale, AZ 85260

## Background and Purpose

The access will be located at the roundabout at $74^{\text {th }}$ Way and Ashler Hills Drive. During the construction of the Project, the existing roundabout/traffic circle will be removed. In addition, an eastbound left turn lane will be added and the existing bike lane will be extended to the proposed entrance. The design of the site driveway and side walk across the driveway should be designed Per the City of Scottsdale Standard Detail Drawings, revised in 2020 based on the following details: COS Driveway Type CL-1, DSPM 5-3.200, and DSPM Sec. 5-3.205. The City's details are also provided in Attachment C. The site will provide approximately 70 parking spaces to accommodate the park.

The park will consist of approximately 8 pickleball courts, 1 basketball court, and a general park area. CivTech estimated the acreages of the general park area to be approximately 6.8 -acres. CivTech is aware that only a portion of the 6.8 -acres will be utilized as a general park; but to be conservative, it was assumed that the general will be the entire 6.8 -acres.

This TIS is part of Floor Associates' application to the City requesting a rezoning of the project site. The purpose of this statement is to document the expected number of daily and peak hour trips generated by the site and analyze the adjacent signalized intersection.

This update is also in response to the neighbor's questions and concerns. An addendum was provided to address the concerns and is included in Attachment J.

## Existing Traffic Conditions

Scottsdale Road is a north-south minor arterial roadway classified by the City of Scottsdale's Functional Classification Map. The roadway is a four (4) lane divided roadway with two (2) travel lanes and a bike lane in each direction and a center 29 -foot raised median. Scottsdale Road begins to the north at Carefree Highway extending south to transition into Drinkwater Boulevard just south of Camelback Road. The posted speed limit is 50 miles per hour ( mph ) within the vicinity of the site.

Ashler Hills Drive is an east-west non-classified roadway. The roadway is mainly a two (2) lane roadway with one (1) lane in each travel direction. Between Scottsdale Road and the roundabout to the east, Ashler Hills Drive provides one (1) eastbound lane, two (2) westbound lanes, a bike lane in each direction, and a center 13 -foot raised median. Ashler Hills Drive begins to the west at $68^{\text {th }}$ Street extending east to become $74^{\text {th }}$ Way at the roundabout. The posted speed limit is 25 mph within vicinity of the site.

The intersection of Scottsdale Road and Ashler Hills Drive operates as a signalized intersection with protected-permitted left turn phasing in the northbound, eastbound, and westbound approaches and protected left turn phasing in the southbound approach. The northbound and southbound approaches are striped to consist of an exclusive left turn lane, two (2) through lanes, a bike lane, and an exclusive right turn lane. The eastbound approach is striped to consists of an exclusive left turn lane, a shared through/right-turn lane, and a bike lane. The westbound approach is striped to consists of an exclusive left turn lane, one (1) through lane, a bike lane, and an exclusive right turn lane. A designated pedestrian crosswalk is provided at each leg of the intersection.

CivTech engaged Field Data Services of Arizona, Inc. on Wednesday, April 14, 2021 peak hour volume turning movement counts were performed from 7:00-9:00 AM and 4:00-6:00 PM and Saturday, April 17, 2021 peak hour volume turning movement counts were performed from 7:00-9:00 AM and 11:00 AM-1:00 PM at Scottsdale Road and Ashler Hills Drive for this project. CivTech also engaged in All Traffic Data for 24-hour approach counts on Ashler Hills Drive between $73{ }^{\text {rd }}$ Street and the roundabout on Thursday, March 17, 2022.

CivTech took historical daily traffic volumes from the City of Scottsdale website Daily Traffic Volume Map to estimate an average annual growth rate. Average daily traffic volumes on Scottsdale Road between Ashler Hills Drive and Dove Valley Road were considered. The location experienced an average annual increase of $0.7 \%$ per year from 2016 to 2018. To be conservative a $1 \%$ annual growth rate ( 1.010 annual expansion factor for the 2022 year) was applied to the 2021 turning movement counts at the intersection of Scottsdale Road and Ashler Hills Drive to obtain 2022 existing traffic volumes. CivTech utilized the 2022 24-hour counts to obtain the AM and PM peak hour through volumes at $74^{\text {th }}$ Way and Existing Driveway located just east of the roundabout. By doing so, the volumes separate the commercial trips from the residential trips traveling along $74^{\text {th }}$ Way.

Saturday peak hour counts at $74^{\text {th }}$ Way and Existing Driveway were not conducted. To obtain the Saturday volumes at $74^{\text {th }}$ Way and Existing Driveway, CivTech compared the PM with Saturday peak hour ins/outs traffic volumes at the east leg of the intersection of Scottsdale Road and Ashler Hills Drive. The results indicate that the eastbound approach (heading northbound on $74^{\text {th }}$ Way) calculated a factor of 1.40 and the westbound (heading southbound on $74^{\text {th }}$ Way) calculated a factor of 0.97 when comparing the PM and Saturday peak hour ins/outs at the east leg of the Scottsdale Road and Ashler Hills Drive. Therefore, the factor was applied to the existing PM peak hour at $74^{\text {th }}$ Way and Existing Driveway to obtain the Saturday peak hour volumes along $74^{\text {th }}$ Way.

The existing traffic volumes observed for this study intersections are presented in Figure 2 for the typical weekday AM, PM, and Saturday peak hours. Traffic volume counts are provided in Attachment D.

Figure 2 - Existing Peak Hour Traffic Volumes


Scottsdale Rd. \& Ashler Hills Dr.


Ashler Hills Dr./74th Way \& Roundabout

## Trip Generation

The potential trip generation for the proposed development was estimated utilizing the Institute of Transportation Engineers (ITE) Trip Generation Manual, $11^{\text {th }}$ Edition and Trip Generation Handbook, $3^{\text {rd }}$ Edition. The ITE Trip Generation Manual contains data collected by various transportation professionals for a wide range of different land uses. The data are summarized in the report and average rates and equations have been established that correlate the relationship between an independent variable that describes the development size and generated trips for each categorized land use. The report provides information for daily and peak hour trips.

ITE Trip Generation Manual provides a Saturday peak hour of generator rates for the park. With Due to the low trip generation rate for the typical weekday AM peak hour and neighbor's concerns of the AM peak hour trips being too low, CivTech assumed the AM peak hour rate to be the same as the Saturday rate. Therefore, a rate of 1.96 was applied to the AM peak hour to calculate the AM peak hour trips for the park.

ITE Trip Generation Manual does not provide trip generation rates for the specific land uses like pickleball court and basketball court. Since a pickleball court highly similar to a tennis court in terms of number of players, it was assumed that the pickleball courts will utilize the tennis court for PM Peak hour trip generation rates. For the AM peak hour, CivTech conducted a survey from 7:00 AM 9:00 AM of vehicle counts utilizing the basketball court and pickleball courts during on Monday, March 21, 2022 at the Thompson Peak Park located on west of Hayden Road south of Thompson Peak Parkway in Scottsdale, Arizona. The park consists of 3 pickleball courts next to 1 basketball court. Based on the observations there were zero basketball users; at approximately 7:45 AM, the basketball court was converted into three additional pickleball courts. Therefore, the rates derived were based on 6 pickleball courts being counted on the field. The highest peak hour based on the observations were between 8:00-9:00 AM. The observation verifies that a total of 35 trips were made during the AM peak hour with 28 inbound trips and 7 outbound trips. With 35 total trips and 6 pickleball courts, results in an AM peak hour rate of 5.83 . It should be noted that not all the players were playing at the same time. There were some people that stood by and waited for their turn to play. Thus, this concluded that the 5.83 would be maximum rate for the pickleball court. To be conservative, the Saturday peak hour for the pickleball courts is assumed to be the same as the AM peak hour.

CivTech prepared the recently approved Traffic Impact Analysis (TIA) for the Legacy Sports Family Entertainment Park in Mesa, Arizona. The park utilized the tennis court trip generation rates to derive trip generation rates for the basketball court. The ratio between the maximum number of players for a basketball game and for a tennis game is 10 to 4 . Therefore, a multiple of $2.5\left(={ }^{10} / 4\right)$ were applied to the tennis court to estimate the basketball court land use for total daily, AM, PM, and Saturday peak hour. Based on the field data stated above, there were zero trips observed for the basketball court. Therefore, the basketball court AM peak hour rate will remain zero.

The anticipated trip generation is summarized in Table 1. Detailed trip generation calculations along with the field data observations are provided in Attachment $\mathbf{E}$.

## CivTech

Table 1 - Trip Generation

| Land Use | ITE <br> Code | ITE Land Use Name |  |  | Quantity Units+ |  |  | AM <br> Distribution |  | PM <br> Distribution |  | SAT <br> Distribution |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | In | Out | In | Out |  |  | Out |
| Park | 411 | Public Park |  |  |  |  |  | 6.80 Acres |  |  | 59\% | 41\% | 55\% | 45\% |  |  | 50\% |
| Pickleball Courts | 490 |  | Tennis Courts |  | 8 Courts |  |  | 80\% | 20\% | 50\% | 50\% |  |  | 20\% |
| Basketball Court | 490 |  | Tennis Courts |  | Courts |  |  | - | - | 50\% | 50\% |  |  | 50\% |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Land Use | ADT |  | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  | Sat Peak Hour |  |  |  |
|  | Rates | Total | Rate | In | Out | Total | Rate | In | Out | Total | Rate | In | Out | Total |
| Park | 13.65 | 92 | 1.96 | 8 | 5 | 13 | 0.11 | 1 | 0 | 1 | 1.96 | 7 | 6 | 13 |
| Pickleball Courts | 30.32 | 242 | 5.83 | 38 | 9 | 47 | 4.21 | 17 | 17 | 34 | 5.83 | 38 | 9 | 47 |
| Basketball Court | 75.80 | 76 | - | 0 | 0 | 0 | 10.53 | 6 | 5 | 11 | 6.63 | 4 | 3 | 7 |
| Total | $\bigcirc$ | 410 | $\square$ | 46 | 14 | 60 | $\bigcirc$ | 24 | 22 | 46 | $\bigcirc$ | 49 | 18 | 67 |

The proposed development is anticipated to generate 410 weekday daily trips, 60 trips during the typical weekday AM peak hour, 46 trips during the typical weekday PM peak hour, and 67 trips during the Saturday peak hour.

## Trip Distribution and Assignment

A single trip distribution pattern was used in order to develop site generated traffic for the new proposed park. Since the existing traffic within the area is a mixture of residential and commercial trips, the park trip distribution was considered to be different from the existing distribution. The trip distribution assumptions were made based on the surrounding residential area. It was assumed that the park will attract majority of the trips from north and south of Scottsdale Road and a small percentage will be on Ashler Hills Drive and $74^{\text {th }}$ Way. The trip distribution percentages used for this analysis are shown in Table 4.

Table 2 - Trip Distribution Percentages

| Roadway | Directions (to/from) | Distribution <br> Percentages |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Scottsdale Road | North | $55 \%$ |  |  |
| Scottsdale Road | South | $40 \%$ |  |  |
| Ashler Hills Drive | West | $3 \%$ |  |  |
| $74^{\text {th }}$ Way | North | $2 \%$ |  |  |
| Total |  |  |  | $\mathbf{1 0 0 \%}$ |

Figure 3 illustrates the trip distribution percentages shown in Table 2 along the roadway network within the study area. The percentages presented in Table $\mathbf{2}$ were applied to the site trips generated to determine the weekday AM, PM, and Saturday peak hour site traffic at the intersections within the study area. Figure 3 illustrates the resulting site generated traffic for the proposed development.

Figure 3 - Site Generated Traffic Volumes


Scottsdale Rd. \& Ashler Hills Dr.


## 2023 Background and Surrounding Development Traffic Volumes

An annual growth rate of $1 \%$ will be utilized to calculate the 2023 background traffic volumes based on the methodology stated above. Thus, an expansion factor of 1.01 was applied to the 2022 existing volumes to retain the 2023 background traffic volumes without surrounding development.

East of the site is an undeveloped vacant land. The parcel is proposed to be 101 townhomes in the future with two (2) accesses, one (1) at the existing driveway and one (1) driveway on $74^{\text {th }}$ Way. To be conservative, CivTech considered the east development to be open by the time the Park is open and generated trips using the ITE $11^{\text {th }}$ Edition trip generation rates for LUC 215. For the Saturday peak hour assumptions, CivTech applied the ITE's Saturday peak hour of generator rates. The resulting trip generation indicated that the east development is anticipated to generate 720 weekday daily trips, with 47 trips ( $15 \mathrm{in} / 32$ out) during the AM peak hour, 57 trips ( $32 \mathrm{in} / 25$ out) during the PM peak hour, and 58 trips ( $28 \mathrm{in} / 30$ out) during the Saturday peak hour. A single trip distribution pattern was provided for the development. Based on the Google Earth Pro aerial, there are multiple commercial developments are to the north of Ashler Hills Drive. Therefore, it was assumed that 63\% of the trip distribution will be on Scottsdale Road north of Ashler Hills Drive. With the Loop 101 Freeway located approximately 8.41 miles to the south, a $35 \%$ trip distribution was assumed to be on Scottsdale Road south of Ashler Hills Drive to represent vehicles traveling long distances to/from work. The remaining 2\% was assumed to be on Ashler Hills Drive west of Scottsdale Road to consider the cut through traffic that are heading to/from the schools located to the northwest. Figure 4 illustrates the resulting site generated traffic for the east development at the study intersections. Figure 5 illustrates the 2023 background traffic volumes (2022 existing grown to $2023+$ east development) at the study intersections. Trip generation calculations for the east development is provided in Attachment F.

Figure 4 - East Development Site Generated Traffic Volumes


Figure 5-2023 Background Traffic Volumes


## 2023 Total Traffic Volumes

2023 total traffic volumes at the site access and the main intersection of Scottsdale Road and Ashler Hills Drive were determined by adding the proposed site generated traffic volumes and east development site generated traffic volumes to the 2023 background traffic volumes. Figure 6 illustrates the resulting 2023 total traffic at the study intersections. Based on the highest peak hour generating less than 50 trips during the AM peak hour and only 56 trips estimated for the Saturday peak hour it was assumed that 70 parking spaces would be sufficient for the park.

Figure 6 - $\mathbf{2 0 2 2}$ Total Traffic Volumes


Scottsdale Rd. \& Ashler Hills Dr.


## 24-Hour Daily Trips

The 24-hour bi-directional counts conducted along Ashler Hills Drive determined that there are approximately 521 total daily trips (269 eastbound approach and 252 westbound approach). The daily volumes were then grown to 2023 year by an expansion factor of 1.010 . Resulting in 527 total daily trips ( 272 eastbound approach and 255 westbound approach). The site generated weekday daily total will add only 410 trips (with $98 \%$ to/from west of the site and $2 \%$ to/from east of the site) and the east development site generated weekday daily total is projected to add 720 trips onto Ashler Hills Drive projecting the average daily to 1,649 total daily trips. The 2023 average daily total for a weekday traffic volume is shown in Figure 7.


Figure 7-2023 Average Daily Total Traffic Volumes with Site \& East Development Traffic

## TRAFFIC IMPROVEMENT AND ANALYSIS

## CAPACITY ANALYSIS

The concept of level of service (LOS) uses qualitative measures that characterize operational conditions within the traffic stream. The individual levels of service are described by factors that include speed, travel time, freedom to maneuver, traffic interruptions, and comfort and convenience. Six (6) levels of service are defined for each type of facility for which analysis procedures are available. They are given letter designations $A$ through $F$, with LOS A representing the best operating conditions and LOS F the worst. Each level of service represents a range of operating conditions. Levels of service for intersections are defined within ranges of average control delay per vehicle, the number of seconds a vehicle can expect to wait due to the presence of a traffic control device. Table 3 lists the level of service criteria for signalized

Table 3 - Intersection Level of Service Criteria

| Level of <br> Service | Control Delay (sec/veh) |  |
| :---: | :---: | :---: |
|  | Signalized | Unsignalized |
| A | $\leq 10$ | $\leq 10$ |
| B | $>10-20$ | $>10-15$ |
| C | $>20-35$ | $>15-25$ |
| D | $>35-55$ | $>25-35$ |
| E | $>55-80$ | $>35-50$ |
| F* | $>80($ or v/c>1) | $>50($ or v/c>1) |

Source: Exhibits 19-8, 20-2, 21-8, and 22-8, Highway Capacity Manual 2016 and unsignalized intersections.

Synchro 11 software using the methodologies of the latest ( $6^{\text {th }}$ ) edition of the Highway Capacity Manual (HCM 2016) will be used to calculate average per-vehicle control delays, from which
movement, approach, and overall intersection levels of service are determined. Signal timing at the intersection of Scottsdale Road and Ashler Hills Drive were provided by the City of Scottsdale Engineer. The capacity analysis for the AM and PM peak hours at the site access, for existing, background (existing grown to 2023 year + east development), and total (background + site) are summarized in Table 4. The Synchro analysis worksheets are included as Attachment G.

Table 4-2023 Levels of Service and Delays

(1) In the existing conditions, the roundabout is a 2-legged intersection. Synchro HCM does analyze 2-legged intersection. Since there are no conflicting movements, this intersection was assumed to operate acceptably during the existing condition.

The results of capacity analysis of the study intersection summarized in Table 4 shows that the proposed site access and the intersection of Scottsdale Road and Ashler Hills Drive is predicted to operate at acceptable levels of service (LOS D or better) with the exception of the westbound approach in during PM and Saturday peak hour during the existing conditions. However, the overall level of service for the intersection is operating at an acceptable level of service of $C$ or better. The delays with the added park traffic in the westbound direction were increased one second or less for the AM, PM and Saturday peak hours. The overall increase in delay for the intersection were 0.4 sec or less for AM, PM and Saturday peak hours.

The basic signal timing plan was utilized for all peak hour analyses. However, based on the City's signal timing sheet, the eastbound through and westbound through lanes maximum split provided was less than the minimum split. The City's Engineer asked CivTech to keep the signal timing consistent to the spreadsheet provided for the existing analysis only. For the No Build and Build conditions, CivTech mitigated the signal timing at the intersection of Scottsdale Road and Ashler Hills Drive to provide 120 seconds of cycle length and adjusted the green time to provide acceptable levels of service at all approaches.

With the mitigation of the signal timing, the intersection of Scottsdale Road and Ashler Hills Drive is expected to operate acceptably.

## Queue Storage Analysis

Adequate turn storage should be supplied on any approach where turn lanes are permitted and/or warranted. A queuing analysis was prepared according to the methodology documented in AASHTO's A Policy on Geometric Design of Highways and Streets. The storage length for a turn lane is typically estimated as the length required to hold the average number of arriving vehicles per two minutes,
where unsignalized. The equations used for the calculations are shown below, and the resulting turn lane storage requirements for the study intersection:

For unsignalized intersections, the storage length for a left turn lane is determined by the following equation:

$$
\text { Storage Length }=\left\{\frac{\ln [P(n>N)]}{\ln \frac{\nu}{c}}-1\right\} \times 25 \text { feet }
$$

as defined in AASHTO's A Policy on Geometric Design of Highways and Streets Equations 9-3 and 9-4. Queue storage queue calculations worksheet is provided in Attachment H.

Table 5 - Queue Storage Lengths

|  | Intersection | Intersection Control | Movement | Queue Storage |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID |  |  |  | Existing ${ }^{(1)}$ | AASHTO | HCM ${ }^{(2)}$ | Recommended |
| 2/A | Ashler Hills Dr./74 Way \& Access A | 1-way stop <br> (SB) | EB Left | TWLTL | $25^{\prime}$ | <25' | 93' |

The results of the queue storage calculations indicate a queue storage of 25 -feet for the eastbound left into the site. Based on Google Earth, there are approximately 230 -feet of storage that can be queue back to the raised median on the west of the driveway. Per the site plan, a queue storage length of 93 -feet was proposed for the eastbound left turn lane.

## Sight Distance Analysis

Adequate sight distance must be provided at intersections and site access driveways to allow safe turning movements. There must be sufficient unobstructed sight distance along both approaches of a street/driveway intersection and across their included corners to allow operators of vehicles to see each other in time to prevent a collision. Along a tangent segment of roadway, the area that is to be unobstructed is a right triangle. The position of the driver about to exit the driveway is one (often called the origin) point of the triangle.

Sigh distance measurement for this Project is based on City of Scottsdale methodology in accordance to Section 5-3C, Intersection \& Driveway Sight Distance Requirements which adhere to ASSHTO's calculation of sight distance. The City of Scottsdale set the point of the driver position at 5 -feet to the right from the center of the driveway, 3.5 feet above the pavement, and a setback of 15 -feet from the inner edge of curb. $74^{\text {th }}$ Way/Ashler Hills Drive is a non-classified road with a posted speed limit of 25 mph ; therefore, the assumed design speed is 5 mph over the posted speed limit. The City of Scottsdale and AASHTO's calculation resulted in the same sight distance measurements. Sight distance calculations according to the City of Scottsdale guidelines are summarized in Table 6.

Table 6 - City of Scottsdale Sight Distance Requirements

| Driveway | Posted Speed Limit/ <br> Design Speed (mph) | Sight Distance Along Roadway |  |
| :---: | :---: | :---: | :---: |
|  | $25 / 30$ | Through Lane | Left Turn Lane |
| Access A | $290^{\prime}$ | $335^{\prime}$ |  |

Sight distance availability for traffic turning onto $74^{\text {th }}$ Way/Ashler Hills Drive from the proposed site driveway (the north leg of the roundabout) was measured on Google Earth Pro and is provided in Exhibit A.

The City of Scottsdale criteria also states, "Sight lines are to be drawn on roadway and landscaping plans to represent the areas that must be free of all objects and topography in excess of 18 inches above the roadway surface, however, certain vegetation will be allowed. Vegetation placed within the sight triangle will be a low variety that remains below 18 inches when mature. Trees can be considered within the triangles as long the canopies are above 8 feet, they are a single trunk variety, and they are not spaced in a configuration that creates a "picket fence" effect."

Sight visibility should be provided at all driveways according to the distances shown in Table 5 and that sight triangles at public intersections are maintained according to Section 5-3 of the City of Scottsdale's Code. All vegetation and trees should be maintained according to the City of Scottsdale's regulations. Sight distance worksheets and Section 5-3 of the City of Scottsdale's Code have been along with AASHTO's sight distance calculations are included within Attachment $\mathbf{H}$.

## Conclusions

From the above, the following can be concluded:

- The proposed park consists of pickleball courts, a basketball court, picnic ramadas, and trails with 70 parking spaces located at Ashler Hills Drive at $74^{\text {th }}$ Drive in the City of Scottsdale, Arizona.
- The proposed development is anticipated to generate 410 weekday daily trips, 60 trips during the typical weekday AM peak hour, 46 trips during the typical weekday PM peak hour, and 67 trips during the Saturday peak hour.
- The 24 -hour bi-directional counts conducted along Ashler Hills Drive determined that there are approximately 521 total daily trips ( 269 eastbound approach and 252 westbound approach). The daily volumes were then grown to 2023 year by an expansion factor of 1.010. Resulting in 527 total daily trips ( 272 eastbound approach and 255 westbound approach). The site generated weekday daily total will add only 410 trips (with $98 \%$ to/from west of the site and $2 \%$ to/from east of the site) and the east development site generated weekday daily total is projected to add 720 trips onto Ashler Hills Drive projecting the average daily to 1,649 total daily trips.
- Based on the highest peak hour generating 60 trips during the AM peak hour and only 67 trips estimated for the Saturday peak hour it was assumed that 70 parking spaces would be sufficient for the park.
- The results of the queue storage calculations indicate a queue storage of 25 -feet for the eastbound left into the site. Based on Google Earth, there are approximately 230 -feet of storage that can be queue back to the raised median on the west of the driveway. Per the site plan, a queue storage length of 93 -feet was proposed for the eastbound left turn lane.

Thank you for allowing CivTech to assist you on this project. Please contact me with any questions you may have on this Traffic Statement.

Sincerely,

## CivTech



David S. Duffy, P.E. Senior Traffic Engineer

Attachments (9)
A. City's Comments and Responses
B. Site Plan
C. COS Standard Detail Drawings
D. Traffic Counts
E. Trip Generation Calculations
F. East Development Trip Generation Calculations
G. Synchro Analyses
H. Queue Storage Calculations
I. Sight Distance Calculations and City's Requirements
J. Ashler Hills Addendum Letter

Exhibit A - Sight Distance Photos

## 1st Submittal

Disposition Codes:
(1) Will Comply
(2) Will Evaluate
(3) Delete Comment
(4) Defer to Consultant/Owner

Reviewer Name, Agency: Phil Kercher \& Parker Murphy, City of Scottsdale

| Item | Review Comment | (Code) \& Response |
| :---: | :---: | :---: |
| 1. | Transportation - The site driveway should be designed in conformance with COS Driveway Type CL-1, COS Standard Detail \#2256. The sidewalk across the driveway should be modified to conform to the driveway detail, not be separated so far from the curb line. DSPM 5-3.200; DSPM Sec. 5-3.205; COS Standard Detail Drawinas - 2020 revision. | (1) Will comply. The design standard details is included as part of the attachments. |
| 2. | Transportation - What speed limit is the sight visibility triangle based upon? | Sight distance triangle is 5 mph over the posted speed limit ( 30 mph ). |
| 3. | Transportation - Staff suggests moving the site driveway west of the traffic circle to improve sight triangle, or at circle but remove center island. Conceptual plan sent to CPM. |  |
| 4. | Traffic Study - Page 1 - Correct title to "74th Way" and remove references to 74th drive throughout the report. | (!) Will comply. |
| 5. | Traffic Study - Page 2 -Remove or modify the statement that "there was a previously approved planned for this location with the location of the driveway on 74th Avenue instead of..." This site is on 74th Way. Staff was not aware of any previously approved plans. | (1) Will comply. |
| 6. | Traffic Study - Page 2 - Remove or modify the statement this is not a traffic analysis. The study contains level of service analyses and is a traffic analysis, not just a trip generation statement. | (1) Will comply. |
| 7. | Traffic Study - Page 4-The trip generation estimates need to include AM peak hour trips for the pickleball courts and basketball courts. If necessary the consultant should do some count at existing City facilities. | (1) CivTech personnel conducted a field study and collected AM peak hour counts for the pickleball and basketball court at the Thompson Peak Park located west of Hayden Road and south of Thompson Peak Parkway. |

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Appendix A
Page 1 of 2

## 1st Submittal

Disposition Codes:
(1) Will Comply
(2) Will Evaluate
(3) Delete Comment
(4) Defer to Consultant/Owner

Reviewer Name, Agency: Phil Kercher \& Parker Murphy, City of Scottsdale

| Item | Review Comment | (Code) \& Response |
| :---: | :---: | :---: |
| 8. | Traffic Study - Provide a trip generation estimate for the undeveloped property just east of the park site using the existing zoning and include these trips in the traffic analysis. | (1) CivTech reached out to Murphy Parker, the City Engineer and rreceived information for the east development. The City does not have a site plan that informed that the development will be townhomes under LUC 215 in the ITE's Trip Generation 11th Edition with 101 DUs. |
| 9. | Traffic Study - The study should comment on the proposed driveway location and necessary sight distance. The study should provide comment on the proposed location at the traffic circle. | (1) CivTech provided a section of the sight distance calculations as well as an exhibit with the sight distance measurements at the roundabout. |
| 10. | Traffic Study - Study should collect traffic data east of the commercial driveways. | (1) new 24-hour bidirectional counts were conducted just east of 73 rd St. and is provided as part of the attachments. |
| 11. | Traffic Study - General, no changes required. ITE Trip Generation 11th Edition should be used be used for future submittals. | (1) analysis has been updated to ITE's Trip Generation, 11th Edition. |
| 12. | Traffic Study - Ensure Synchro analysis utilizes existing signal timing as provided. Please resubmit the revise application requirements and additional information identified in Attachment A. Resubmittal Checklist, and a written summary response addressing the comments/corrections identified above as soon as possible for future review. | (1) CivTech utilized latest signal timing provided by the City. CivTech reached out to the City's Engineer and confirmed that the "Basic Timing Plan" can bee used by it must match the timing sheet in the existing condition analysis even if the green time are less than the minimum time for the eastbound and westbound through movements. The City Engineer suggests that mitigation of the green time should happen in the "no-build" and "build" analysis. |

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Appendix A



-     - 




FIGURE 5-3.34 ROUNDABOUT SIGHT DISTANCE

## STREET ACCESS AND DRIVEWAYS

Driveway types are determined by land use type and street classification. The standards for these driveway types are illustrated in Figure 5-3.38 through Figure 53.43. Refer to Figure 5-3.39 for driveway grade standards.

## DRIVEWAY SPACING

Standard and minimum driveway spacing will generally conform to the following standards. This minimum spacing applies to proposed site driveway separation as well
as separation from existing or planned driveways and streets on adjacent parcels. The spacing is measured to the driveway or street centerline.

| STREET TYPE | STANDARD DRIVEWAY <br> SPACING | MINIMUM DRIVEWAY <br> SPACING |
| :--- | :---: | :---: |
| Local Residential / Local <br> Collector | 50 feet | 50 feet |
| Local Industrial / Local <br> Commercial | 165 feet | 125 feet |
| Minor Collector | 165 feet | 125 feet |
| Major Collector | 250 feet | 150 feet |
| Minor Arterial | 330 feet | 250 feet |
| Major Arterial | 500 feet | 300 feet |

FIGURE 5-3.35 DRIVEWAY SPACING
Standard driveway spacing criteria shall apply for all new driveways where there are no conflicts with existing driveway and street intersections, site frontage is adequate, and there are no conflicts with natural features or drainage structures. The minimum driveway spacing may be allowed when approved by Transportation staff where those conflicts noted above exist or other site plan associated issues do not allow the standard driveway spacing to be implemented. In locations where the standard driveway spacing cannot be achieved, a deceleration lane may be required to mitigate the impact of the closer driveway spacing.
For sites that have frontage on two streets, primary access should be onto the minor street frontage. A maximum of two driveway openings is permitted to a site or parcel from the abutting street(s). The Transportation Department may permit additional driveway entrances when projected travel demands indicate it is in the interests of good traffic operation, and when adequate street frontage exists to maintain the above guidelines.
Where new development adjoins other similarly zoned property or compatible land uses, a cross access easement may be required to permit vehicular movement between the parcels or to reduce the number of access points required onto the adjacent public street. Combining driveways reduces the number of conflict points for pedestrians, bicyclists, and other vehicles. This may be required regardless of the development status of the adjoining property, unless the cross access is determined to be unfeasible by city staff.
New driveways on collector and arterial streets in areas that do not have raised medians shall align with existing or planned driveways and street intersections to avoid creating interlocking left turns and other conflicts. Offsets in the driveway centerlines may be allowed up to 6 feet. If the driveways cannot be aligned, the driveways should be offset a minimum distance of 125 feet along streets without a center turn lane, and a minimum 250 feet along streets with a center turn lane. When site driveway locations are modified, any existing driveways that are not going to be utilized for access must be removed and replaced with curb, gutter, and sidewalk to match the adjacent improvements.

## DRIVEWAY LOCATIONS

A new access driveway will not be allowed (measured to the driveway centerline):
A. Within 30 feet of any commercial property line, except when it is a joint-use driveway serving two abutting commercial properties and access agreements have been exchanged between, and recorded by, the two abutting property owners;
B. When the total width of all driveways serving a property exceeds 50 percent of the curb line frontage;
C. Within 50 feet of the rights-of-way line of an intersecting non-arterial street;
D. Within 100 feet of the rights-of-way line of an intersecting arterial street;
E. Within 100 feet of an approved median opening location on an arterial street;
F. Less than the minimum spacing as established under Section 5-3.201;

## VEHICULAR NON-ACCESS EASEMENT

For proper control of driveway access, a vehicular non-access easement (V.N.E.) is to be granted to the city, except at approved access points, along all collector and arterial streets when abutting property develops.

## RESIDENTIAL DRIVEWAYS

A. Single-family Residential Development

Driveways serving single-family residential units should be S-1 type driveways as shown in Figure 5-3.40. Only one driveway per lot street frontage is allowed except where the street frontage is of sufficient length to maintain a separation of 50 feet between driveways. The minimum driveway length is 18 feet, measured from the face of the garage opening to the back of sidewalk or the back of curb if no sidewalk is provided. Refer to Section 2-2.308 for additional discussion on driveways. Refer to Standard Detail Drawings (2200 Series) for access ramp design requirements.
B. Multi-family Residential Development

Driveways serving multi-family residential units should be CL and CH type driveways, as shown in Figure 5-3.41 through Figure 5-3.44. Type CL-1 and CL-2 are low-volume driveways to be used on local streets. Type $\mathrm{CH}-1,-2$ and -3 are high volume driveways to be used on collector and arterial streets. CL type driveways may be required along urban character collector and arterial streets with higher pedestrian traffic. The minimum driveway length is 50 feet, measured from the entrance to the off-street parking area to the back of sidewalk, or to the back of curb if no sidewalk is provided. Refer to Standard Detail Drawings (2200 Series) for access ramp design requirements.
C. Limitations on Residential Access

Residential properties that have frontage on a local street, an arterial, or collector street are limited to local street access.
In some instances, residential parcels fronting only on arterial or collector streets may be given access if alternate public access is not available. When such access is allowed, the driveway must be circular, or it must have a turn-around area to ensure there is no need for backing onto the street.

## NON-RESIDENTIAL DRIVEWAYS

Driveways for commercial and industrial development are shown on Figure 5-3.41 through Figure 5-3.44. The minimum length for a commercial or industrial driveway is 50 feet, measured from the entrance to the off-street parking area to the back of sidewalk or the back of curb if no sidewalk is provided. Driveway designs need to include a level path of travel across the driveway for pedestrians in conformance with ADA requirements.

## A. Commercial Driveways

The "CL" and "CH" type driveways are designed to serve commercial properties. A "CL" type driveway is used for low-volume driveways on low volume streets. A "CH" type driveway is used for driveways on arterials, major collectors and high volume minor collectors, or at other locations when required by the Transportation Department. The $\mathrm{CH}-2$ and $\mathrm{CH}-3$ driveways are used at all access driveways opposite median openings. CL type driveways may be required along urban character collector and arterial streets with higher pedestrian traffic. Refer to Standard Detail Drawings (2200 Series) for access ramp design requirements.
B. Industrial Driveways

The CL-1 and CH-1 type driveways are typically used to serve industrial properties. Normally industrial access is not permitted on arterial or major collector streets; however, if such access is allowed, commercial driveway standards apply. Refer to Standard Detail Drawings (2200 Series) for access ramp design requirements.

Intersection Turning Movement Prepared by:
Field Data Services of Arizona, Inc.


## veracitytraffic group

N-S STREET: Scottsdale Rd
DATE: 04/14/21
LOCATION: Scottsdale
E-W STREET: Ashler Hills Dr
DAY: WEDNESDAY
PROJECT\# 21-1247-001

| LANES: | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \mathrm{NL} \\ 1 \end{gathered}$ | NT 2 | NR 1 | SL 1 | $\begin{gathered} \mathrm{ST} \\ 1 \end{gathered}$ | SR 2 | EL 1 | ET 1 | $\begin{gathered} \text { ER } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WL } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WT } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 6:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00 AM | 45 | 122 | 3 | 1 | 136 | 2 | 1 | 0 | 13 | 10 | 1 | 1 | 335 |
| 7:15 AM | 18 | 144 | 5 | 1 | 145 | 2 | 4 | 0 | 25 | 5 | 0 | 1 | 350 |
| 7:30 AM | 11 | 117 | 4 | 2 | 172 | 7 | 7 | 1 | 17 | 9 | 0 | 2 | 349 |
| 7:45 AM | 45 | 180 | 13 | 0 | 176 | 12 | 14 | 1 | 30 | 5 | 0 | 1 | 477 |
| 8:00 AM | 33 | 146 | 14 | 4 | 151 | 8 | 14 | 2 | 44 | 14 | 1 | 5 | 436 |
| 8:15 AM | 10 | 170 | 22 | 1 | 156 | 6 | 4 | 0 | 22 | 19 | 1 | 2 | 413 |
| 8:30 AM | 5 | 186 | 20 | 2 | 185 | 1 | 3 | 3 | 8 | 32 | 0 | 5 | 450 |
| 8:45 AM | 4 | 210 | 23 | 4 | 193 | 1 | 2 | 4 | 10 | 20 | 0 | 5 | 476 |
| 9:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 171 | 1275 | 104 | 15 | 1314 | 39 | 49 | 11 | 169 | 114 | 3 | 22 | 3286 |
| Approach \% | 11.03 | 82.26 | 6.71 | 1.10 | 96.05 | 2.85 | 21.40 | 4.80 | 73.80 | 82.01 | 2.16 | 15.83 |  |
|  | 1350 | $/$ | 1346 | 1368 | $/$ | 1597 | 229 | $/$ | 130 | 139 | $/$ | 213 |  |

AM Peak Hr Begins at: 745 AM
PEAK

| Volumes | 93 | 682 | 69 | 7 | 668 | 27 | 35 | 6 | 104 | 70 | 2 | 13 | 1776 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Approach \% | 11.02 | 80.81 | 8.18 | 1.00 | 95.16 | 3.85 | 24.14 | 4.14 | 71.72 | 82.35 | 2.35 | 15.29 |  | PEAK HR.


CONTROL:
COMMENT 1:
GPS:
Signal
33.777534, -111.925847

## I ntersection Turning Movement



| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 79 | 1795 | 213 | 39 | 1344 | 20 | 30 | 13 | 71 | 444 | 24 | 49 | 4121 |
| Approach \% | 3.79 | 86.01 | 10.21 | 2.78 | 95.79 | 1.43 | 26.32 | 11.40 | 62.28 | 85.88 | 4.64 | 9.48 |  |
| App/Depart | 2087 | 1 | 1874 | 1403 | 1 | 1859 | 114 | 1 | 265 | 517 |  | 12 |  |

PM Peak Hr Begins at: $\quad 400$ PM
PEAK

| Volumes | 39 | 927 | 115 | 21 | 705 | 10 | 18 | 8 | 36 | 248 | 13 | 28 | 2168 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Approach \% | 3.61 | 85.75 | 10.64 | 2.85 | 95.79 | 1.36 | 29.03 | 12.90 | 58.06 | 85.81 | 4.50 | 9.69 |  |

PEAK HR.
FACTOR
CONTROL: Signal
COMMENT 1: 0
GPS:
33.777534, -111.925847

Intersection Turning Movement Prepared by:
Field Data Services of Arizona, Inc.


## veracitytraffic group

| N-S STREET: | Scottsdale Rd | DATE: $04 / 17 / 21$ | LOCATION: |
| :--- | :--- | :---: | :--- |
| E-W STREETtsdale $:$ | Ashler Hills Dr | DAY: SATURDAY | PROJECT\# |
| 21-1247-003 |  |  |  |


| LANES: | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NL 1 | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | NR 1 | SL 1 | $\begin{gathered} \mathrm{ST} \\ 1 \end{gathered}$ | SR 2 | EL 1 | ET 1 | $\begin{gathered} \text { ER } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WL } \\ 1 \end{gathered}$ | WT | WR |  |
| 6:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00 AM | 0 | 78 | 7 | 0 | 64 | 1 | 1 | 0 | 3 | 3 | 0 | 0 | 157 |
| 7:15 AM | 4 | 76 | 8 | 2 | 72 | 0 | 2 | 0 | 2 | 6 | 0 | 1 | 173 |
| 7:30 AM | 4 | 100 | 14 | 4 | 85 | 1 | 3 | 0 | 9 | 6 | 0 | 3 | 229 |
| 7:45 AM | 9 | 124 | 16 | 3 | 82 | 1 | 2 | 2 | 9 | 10 | 0 | 4 | 262 |
| 8:00 AM | 9 | 154 | 26 | 3 | 129 | 1 | 1 | 4 | 1 | 17 | 0 | 7 | 352 |
| 8:15 AM | 9 | 118 | 21 | 4 | 114 | 1 | 1 | 1 | 8 | 20 | 5 | 9 | 311 |
| 8:30 AM | 8 | 152 | 19 | 2 | 128 | 0 | 5 | 0 | 5 | 25 | 1 | 10 | 355 |
| 8:45 AM | 15 | 177 | 26 | 5 | 138 | 2 | 4 | 3 | 11 | 26 | 0 | 3 | 410 |
| 9:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 58 | 979 | 137 | 23 | 812 | 7 | 19 | 10 | 48 | 113 | 6 | 37 | 2249 |
| Approach \% | 4.94 | 83.39 | 11.67 | 2.73 | 96.44 | 0.83 | 24.68 | 12.99 | 62.34 | 72.44 | 3.85 | 23.72 |  |
|  |  | 1174 | 1 | 1035 | 842 | 1 | 973 | 77 | 1 | 170 | 156 | 1 | 71 |

AM Peak Hr Begins at: 800 AM
PEAK

| Volumes | 41 | 601 | 92 | 14 | 509 | 4 | 11 | 8 | 25 | 88 | 6 | 29 | 1428 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach \% | 5.59 | 81.88 | 12.53 | 2.66 | 96.58 | 0.76 | 25.00 | 18.18 | 56.82 | 71.54 | 4.88 | 23.58 |  | PEAK HR.


CONTROL:
COMMENT 1:
GPS:

## Signal

33.777534, -111.925847

## I ntersection Turning Movement

## Field Data Services of Arizona, Inc. <br> 520.316.6745 <br> veracitytraffic group

| N-S STREET: | Scottsdale Rd | DATE: 04/17/21 | LOCATION: Scottsdale |
| :--- | :--- | :---: | :--- |
| E-W STREET: | Ashler Hills Dr | DAY: SATURDAY | PROJECT\# |
| 21-1247-003 |  |  |  |


|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LANES: | NL 1 | NT 2 | NR 1 | SL 1 | ST 1 | SR 2 | EL 1 | ET 1 | $\begin{gathered} \text { ER } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WL } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WT } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 10:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM | 14 | 209 | 25 | 11 | 199 | 1 | 4 | 1 | 9 | 47 | 2 | 2 | 524 |
| 11:15 AM | 13 | 216 | 39 | 13 | 198 | 5 | 2 | 3 | 14 | 69 | 2 | 6 | 580 |
| 11:30 AM | 10 | 228 | 34 | 8 | 197 | 2 | 5 | 2 | 13 | 59 | 4 | 4 | 566 |
| 11:45 AM | 16 | 256 | 44 | 10 | 190 | 1 | 1 | 3 | 11 | 57 | 3 | 10 | 602 |
| 12:00 PM | 17 | 229 | 41 | 4 | 194 | 4 | 5 | 0 | 8 | 49 | 4 | 12 | 567 |
| 12:15 PM | 13 | 213 | 38 | 10 | 200 | 0 | 4 | 3 | 5 | 63 | 0 | 8 | 557 |
| 12:30 PM | 21 | 214 | 43 | 12 | 178 | 3 | 4 | 1 | 10 | 49 | 2 | 9 | 546 |
| 12:45 PM | 11 | 247 | 30 | 7 | 189 | 5 | 4 | 3 | 6 | 62 | 7 | 10 | 581 |
| 1:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 115 | 1812 | 294 | 75 | 1545 | 21 | 29 | 16 | 76 | 455 | 24 | 61 | 4523 |
| Approach \% | 5.18 | 81.58 | 13.24 | 4.57 | 94.15 | 1.28 | 23.97 | 13.22 | 62.81 | 84.26 | 4.44 | 11.30 |  |
| App/Depart | 2221 | / | 1902 | 1641 | / | 2076 | 121 | 1 | 385 | 540 | / | 160 |  |

PM Peak Hr Begins at: 1115 AM
PEAK

| Volumes | 56 | 929 | 158 | 35 | 779 | 12 | 13 | 8 | 46 | 234 | 13 | 32 | 2315 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

PEAK HR.
FACTOR: | $0.904 \quad \left\lvert\, \begin{array}{lllll} & 0.956 & 0.838 & 0.906 & \mid\end{array}\right.$
CONTROL: Signal
COMMENT 1: 0
GPS:
33.777534, -111.925847

|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Date: 3/17/2022 |  |  |  |  |  |  |
| Start Time: 12:00:00 AM |  |  |  |  |  |  |
| Site Code: 1 |  |  |  |  |  |  |
| Station ID: |  |  |  |  |  |  |
| Location 1: ASHLER HILLS DR E.O 73RD ST |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Date | Time | EB | WB |  |  |  |
| 3/17/2022 | 12:00 AM | 1 | 1 |  |  |  |
| 3/17/2022 | 12:15 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 12:30 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 12:45 AM | 2 | 0 |  |  |  |
| 3/17/2022 | 01:00 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 01:15 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 01:30 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 01:45 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 02:00 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 02:15 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 02:30 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 02:45 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 03:00 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 03:15 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 03:30 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 03:45 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 04:00 AM | 1 | 1 |  |  |  |
| 3/17/2022 | 04:15 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 04:30 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 04:45 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 05:00 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 05:15 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 05:30 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 05:45 AM | 1 | 1 |  |  |  |
| 3/17/2022 | 06:00 AM | 0 | 2 |  |  |  |
| 3/17/2022 | 06:15 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 06:30 AM | 0 | 0 |  |  |  |
| 3/17/2022 | 06:45 AM | 0 | 0 | EB | WB | Total |
| 3/17/2022 | 07:00 AM | 1 | 1 |  |  |  |
| 3/17/2022 | 07:15 AM | 0 | 2 |  |  |  |
| 3/17/2022 | 07:30 AM | 2 | 2 |  |  |  |
| 3/17/2022 | 07:45 AM | 3 | 3 |  |  |  |
| 3/17/2022 | 08:00 AM | 0 | 2 | 6 | 8 | 14 |
| 3/17/2022 | 08:15 AM | 1 | 1 | 5 | 9 | 14 |
| 3/17/2022 | 08:30 AM | 4 | 3 | 6 | 8 | 14 |
| 3/17/2022 | 08:45 AM | 1 | 4 | 8 | 9 | 17 |
| 3/17/2022 | 09:00 AM | 3 | 5 | 6 | 10 | 16 |
| 3/17/2022 | 09:15 AM | 3 | 5 |  |  |  |
| 3/17/2022 | 09:30 AM | 2 | 7 |  |  |  |
| 3/17/2022 | 09:45 AM | 7 | 2 |  |  |  |
| 3/17/2022 | 10:00 AM | 3 | 9 |  |  |  |
| 3/17/2022 | 10:15 AM | 10 | 6 |  |  |  |
| 3/17/2022 | 10:30 AM | 5 | 6 |  |  |  |
| 3/17/2022 | 10:45 AM | 7 | 6 |  |  |  |
| 3/17/2022 | 11:00 AM | 6 | 5 |  |  |  |


| 3/17/2022 | 11:15 AM | 2 | 4 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3/17/2022 | 11:30 AM | 3 | 7 |  |  |  |
| 3/17/2022 | 11:45 AM | 6 | 7 |  |  |  |
| 3/17/2022 | 12:00 PM | 7 | 4 |  |  |  |
| 3/17/2022 | 12:15 PM | 5 | 7 |  |  |  |
| 3/17/2022 | 12:30 PM | 9 | 6 |  |  |  |
| 3/17/2022 | 12:45 PM | 7 | 8 |  |  |  |
| 3/17/2022 | 01:00 PM | 4 | 4 |  |  |  |
| 3/17/2022 | 01:15 PM | 5 | 6 |  |  |  |
| 3/17/2022 | 01:30 PM | 1 | 4 |  |  |  |
| 3/17/2022 | 01:45 PM | 7 | 8 |  |  |  |
| 3/17/2022 | 02:00 PM | 7 | 6 |  |  |  |
| 3/17/2022 | 02:15 PM | 7 | 7 |  |  |  |
| 3/17/2022 | 02:30 PM | 4 | 5 |  |  |  |
| 3/17/2022 | 02:45 PM | 1 | 3 |  |  |  |
| 3/17/2022 | 03:00 PM | 3 | 2 |  |  |  |
| 3/17/2022 | 03:15 PM | 5 | 3 |  |  |  |
| 3/17/2022 | 03:30 PM | 4 | 3 |  |  |  |
| 3/17/2022 | 03:45 PM | 8 | 6 | EB | WB | Total |
| 3/17/2022 | 04:00 PM | 10 | 1 |  |  |  |
| 3/17/2022 | 04:15 PM | 6 | 3 |  |  |  |
| 3/17/2022 | 04:30 PM | 5 | 9 |  |  |  |
| 3/17/2022 | 04:45 PM | 4 | 3 |  |  |  |
| 3/17/2022 | 05:00 PM | 1 | 3 | 25 | 16 | 41 |
| 3/17/2022 | 05:15 PM | 6 | 7 | 16 | 18 | 34 |
| 3/17/2022 | 05:30 PM | 6 | 3 | 16 | 22 | 38 |
| 3/17/2022 | 05:45 PM | 11 | 7 | 17 | 16 | 33 |
| 3/17/2022 | 06:00 PM | 8 | 9 | 24 | 20 | 44 |
| 3/17/2022 | 06:15 PM | 7 | 2 |  |  |  |
| 3/17/2022 | 06:30 PM | 2 | 2 |  |  |  |
| 3/17/2022 | 06:45 PM | 3 | 8 |  |  |  |
| 3/17/2022 | 07:00 PM | 4 | 2 |  |  |  |
| 3/17/2022 | 07:15 PM | 3 | 2 |  |  |  |
| 3/17/2022 | 07:30 PM | 1 | 3 |  |  |  |
| 3/17/2022 | 07:45 PM | 2 | 0 |  |  |  |
| 3/17/2022 | 08:00 PM | 3 | 0 |  |  |  |
| 3/17/2022 | 08:15 PM | 4 | 1 |  |  |  |
| 3/17/2022 | 08:30 PM | 3 | 3 |  |  |  |
| 3/17/2022 | 08:45 PM | 5 | 1 |  |  |  |
| 3/17/2022 | 09:00 PM | 1 | 0 |  |  |  |
| 3/17/2022 | 09:15 PM | 3 | 2 |  |  |  |
| 3/17/2022 | 09:30 PM | 2 | 0 |  |  |  |
| 3/17/2022 | 09:45 PM | 4 | 0 |  |  |  |
| 3/17/2022 | 10:00 PM | 1 | 0 |  |  |  |
| 3/17/2022 | 10:15 PM | 1 | 2 |  |  |  |
| 3/17/2022 | 10:30 PM | 2 | 4 |  |  |  |
| 3/17/2022 | 10:45 PM | 1 | 1 |  |  |  |
| 3/17/2022 | 11:00 PM | 0 | 0 |  |  |  |
| 3/17/2022 | 11:15 PM | 0 | 0 |  |  |  |
| 3/17/2022 | 11:30 PM | 1 | 0 |  |  |  |
| 3/17/2022 | 11:45 PM | 1 | 0 |  |  |  |
|  | Total | 269 | 252 |  |  |  |


| Start | 17-Mar-22 |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Thu | EB | WB |  |  |  |  |  |  | Total |
| 12:00 AM |  | 3 | 1 |  |  |  |  |  |  | 4 |
| 01:00 |  | 0 | 0 |  |  |  |  |  |  | 0 |
| 02:00 |  | 0 | 0 |  |  |  |  |  |  | 0 |
| 03:00 |  | 0 | 0 |  |  |  |  |  |  | 0 |
| 04:00 |  | 1 | 1 |  |  |  |  |  |  | 2 |
| 05:00 |  | 1 | 1 |  |  |  |  |  |  | 2 |
| 06:00 |  | 0 | 2 |  |  |  |  |  |  | 2 |
| 07:00 |  | 6 | 8 |  |  |  |  |  |  | 14 |
| 08:00 |  | 6 | 10 |  |  |  |  |  |  | 16 |
| 09:00 |  | 15 | 19 |  |  |  |  |  |  | 34 |
| 10:00 |  | 25 | 27 |  |  |  |  |  |  | 52 |
| 11:00 |  | 17 | 23 |  |  |  |  |  |  | 40 |
| 12:00 PM |  | 28 | 25 |  |  |  |  |  |  | 53 |
| 01:00 |  | 17 | 22 |  |  |  |  |  |  | 39 |
| 02:00 |  | 19 | 21 |  |  |  |  |  |  | 40 |
| 03:00 |  | 20 | 14 |  |  |  |  |  |  | 34 |
| 04:00 |  | 25 | 16 |  |  |  |  |  |  | 41 |
| 05:00 |  | 24 | 20 |  |  |  |  |  |  | 44 |
| 06:00 |  | 20 | 21 |  |  |  |  |  |  | 41 |
| 07:00 |  | 10 | 7 |  |  |  |  |  |  | 17 |
| 08:00 |  | 15 | 5 |  |  |  |  |  |  | 20 |
| 09:00 |  | 10 | 2 |  |  |  |  |  |  | 12 |
| 10:00 |  | 5 | 7 |  |  |  |  |  |  | 12 |
| 11:00 |  | 2 | 0 |  |  |  |  |  |  | 2 |
| Total |  | 269 | 252 |  |  |  |  |  |  | 521 |
| Percent |  | 51.6\% | 48.4\% |  |  |  |  |  |  |  |
| AM Peak | - | 10:00 | 10:00 | - | - | - | - | - | - | 10:00 |
| Vol. | - | 25 | 27 | - | - | - | - | - | - | 52 |
| PM Peak | - | 12:00 | 12:00 | - | - | - | - | - | - | 12:00 |
| Vol. | - | 28 | 25 | - | - | - | - | - | - | 53 |
| Grand Total |  | 269 | 252 |  |  |  |  |  |  | 521 |
| Percent |  | 51.6\% | 48.4\% |  |  |  |  |  |  |  |
| ADT |  | ADT 521 |  |  |  |  |  |  |  |  |

## Methodology Overview

This form facilitates trip generation estimation using data within the Institute of Transportation Engineer's (ITE) Trip Generation Manual, 11th Edition and methodology described within ITE's Trip Generation Handbook, 3rd Edition. These references will be referred to as Manual and Handbook, respectively. The Manual contains data collected by various transportation professionals for a wide range of different land uses, with each land use category represented by a land use code (LUC). Average rates and equations have been established that correlate the relationship between an independent variable that describes the development size and generated trips for each categorized LUC in various settings and time periods. The Handbook indicates an established methodology for how to use data contained within the Manual when to use the fitted curve instead of the average rate and when to adjustments to the volume of trips are appropriate and how to do so. The methodology steps are represented visually in boxes in Figure 3.1. This worksheet applies calculations for each box if applicable.

Box 1 - Define Study Site Land Use Type \& Site Characteristics
The analyst is to pick an appropriate LUC(s) based on the subject's zoning/land use(s)/future land use(s). The size of the land use(s) is described in reference to an independent variable(s) specific to (each) the land use (example: 1,000 square feet of building area is relatively common).

Land Use Types and Size

| Proposed Use | Amount Units | ITE LUC | ITE Land Use Name |
| :---: | :---: | :---: | :---: |
| Park | 6.800 Acres | 411 |  |
| Pickleball | 8 Courts | 490 | Public Park |
| Basketball | 1 Courts | 490 | Tennis Courts |

## Box 2 - Define Site Context

Context assessment is to "simply determine whether the study sites is in a multimodal setting" and "could have persons accessing the site by walking, bicycling, or riding transit." This assessment is used in Box 4. The Manual separates data into 4 setting categories - Rural, General Urban/Suburban, Dense Multi-Urban Use and Center City Core. This worksheet uses the following abbreviations, respectively: R, G, D, and C. The Manual does not have data for all settings of all land use codes. See the table on the next page titled "Site Context and Time Periods" - if this table is not provided, the "General Urban/Suburban" setting is used by default.

Box 3 - Define Analysis Objectives Types of Trips \& Time Period
This tool will focus on vehicular trips for a 24-hour period on a typical weekday as well as its AM peak hour and PM peak hour. Other time period(s) may be of interest.
Site Context and Time Periods - Actual Setting, Setting Data Available for LUC, Setting Used in Analyses

| Proposed Use | Setting |  | ADT |  | AM Peak Hour |  | PM Peak Hour |  | Saturday |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Available | Used | Available | Used | Available | Used | Available | Used |
| Park |  | G | G | G | G | G | G | G |  | N/A |
| Pickleball | Telletal <br> Urhon/Cuhurban | G | G | G |  | N/A | G | G |  | N/A |
| Basketball | Lurbon/Suburbon | G | G | G |  | N/A | G | G |  | N/A |

If the desired setting is not available within the Manual, adjustments may be made in Boxes 6 through 8 .

Box 4 - Is Study Site Multimodal?
Per the Handbook, "if the objective is to establish a local trip generation rate for a particular land use or study site, the simplified approach (Box 9 ) may be acceptable but the Box 5 through 8 approach is required if the study site is located in an infill setting, contains a mix of uses on-site, or is near significant transit service."

Box 5/Box 9-Estimate Baseline Trips/Estimate Vehicular Trips (Determine Equation)
Vehicle trips are estimated using rates/equations applicable to each LUC. When the appropriate graph has a fitted curve, the Handbook has a process (Figure 4.2 ) to determine when to use it versus using the weighted average rate or collecting local data. The methodology requires for engineering judgement in some circumstances and permits engineering judgement to override or make adjustments when appropriate to best project (example 1: study site is expected to operate differently than data in the applicable land use code - such as restaurant that is closed in the morning or in the evening; example 2: LUC data in a localized area fails to be represented by the typically selected fitted curve/weighted average rate - a small shop/LUC 820 , AM peak hour is skewed by the high $y$-intercept).

Equation Type: Equation Used [Equated Rate] (Type Abbreviations: Weighted Average Rate ("WA"), Fitted Curve ("FC"), or Custom ("C") )

| Proposed Use | ADT | AM Peak Hour | PM Peak Hour | Saturday |
| :---: | :---: | :---: | :---: | :---: |
| Park | FC: $\mathrm{T}=0.64{ }^{*} \mathrm{X}+88.46$ [13.65] | C: $\mathrm{T}=\mathrm{X}^{*} 1.96$ [1.96] | WA: $\mathrm{T}=\mathrm{X}^{*} 0.11$ [0.11] | C: T=X*1.96 [1.96] |
| Pickleball | WA: $\mathrm{T}=\mathrm{X}^{\star} 30.32$ [30.32] | $\mathrm{C}: \mathrm{T}=\mathrm{X}^{*} 5.83$ [5.83] | WA: $\mathrm{T}=\mathrm{X}^{*} 4.21$ [4.21] | $\mathrm{C}: \mathrm{T}=\mathrm{X}^{*} 5.83$ [5.83] |
| Basketball | C: T=X*55.8 [75.80] | C: $\mathrm{T}=\mathrm{X}^{*} 0[0.00]$ | C: $\mathrm{T}=\mathrm{X}^{\star} 10.525$ [10.53] | C: $\mathrm{T}=\mathrm{X}^{\star} 6.63$ [6.63] |

Box 5/Box 9 -Estimate Baseline Trips/Estimate Vehicular Trips (Apply Equations and in/out Distributions)

| Proposed Use | ADT |  |  |  | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  | Saturday |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \% In | In | Out | Total | \% In | In | Out | Total | \% In | In | Out | Total | \% In | In | Out | Total |
| Park | 50\% | 46 | 46 | 92 | 59\% | 8 | 5 | 13 | 55\% | 1 | 0 | 1 | 50\% | 7 | 6 | 13 |
| Pickleball | 50\% | 121 | 121 | 242 | 80\% | 38 | 9 | 47 | 50\% | 17 | 17 | 34 | 80\% | 38 | 9 | 47 |
| Basketball | 50\% | 38 | 38 | 76 | 0\% | 0 | 0 | 0 | 50\% | 6 | 5 | 11 | 50\% | 4 | 3 | 7 |
| Totals |  | 205 | 205 | 410 |  | 46 | 14 | 60 |  | 24 | 22 | 46 |  | 49 | 18 | 67 |


| Monday, March 21, 2022 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Basketball |  |  |  |  |  |
| Time |  |  | Carpool? | Number of Vehicle | Number of People |
|  | Arrival | Departure |  |  |  |
| 7:00 AM |  |  |  |  |  |
| 7:05 AM |  |  |  |  |  |
| 7:10 AM |  |  |  |  |  |
| 7:15 AM |  |  |  |  |  |
| 7:20 AM |  |  |  |  |  |
| 7:25 AM |  |  |  |  |  |
| 7:30 AM |  |  |  |  |  |
| 7:35 AM |  |  |  |  |  |
| 7:40 AM |  |  |  |  |  |
| 7:45 AM |  |  |  |  |  |
| 7:50 AM |  |  |  |  |  |
| 7:55 AM |  |  |  |  |  |
| 8:00 AM |  |  |  |  |  |
| 8:05 AM |  |  |  |  |  |
| 8:10 AM |  |  |  |  |  |
| 8:15 AM |  |  |  |  |  |
| 8:20 AM |  |  |  |  |  |
| 8:25 AM |  |  |  |  |  |
| 8:30 AM |  |  |  |  |  |
| 8:35 AM |  |  |  |  |  |
| 8:40 AM |  |  |  |  |  |
| 8:45 AM |  |  |  |  |  |
| 8:50 AM |  |  |  |  |  |
| 8:55 AM |  |  |  |  |  |
| 9:00 AM |  |  |  |  |  |


| Pickleball |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Time |  |  | Carpool? | Number of Vehicle | Number of People |
|  | Arrival | Departure |  |  |  |
| 7:00 AM | $y$ |  |  | 1 |  |
| 7:05 AM | $y$ |  | y | 1 | 2 |
| 7:10 AM | $y$ |  |  | 1 | 1 |
| 7:15 AM | $y, y$ |  |  | 1,1 | 1,1 |
| 7:20 AM | $y$ |  |  | 1 | 1 |
| 7:25 AM | y (D.O) | y |  | 1,1 | 1,1 |
| 7:30 AM | $y, y, y$ |  |  | 1,1,1 | 1,1,1 |
| 7:35 AM | $y, y$ |  | n, y | 1,1 | 1,2 |
| 7:40 AM | y |  |  | 1 | 1 |
| 7:45 AM | $y$ |  |  | 1 | 1 |
| 7:50 AM |  | $y$ |  | 1 |  |
| 7:55 AM | $y, y, y, y$ | $y$ | $y, n, n, n$ | 1, 1, 1, 1, 1 | 2, 1, 1, 1, 1 |
| 8:00 AM | $y, y, y, y$ |  |  | 1,1,1,1 | 1, 1, 1, 1 |
| 8:05 AM | $y, y, y$ (D.O) | $y$ |  | 1, 1, 1, 1 | 1, 1, 1, 1 |
| 8:10 AM | y |  | $y$ | 1 | 2 |
| 8:15 AM | $y, y, y$ |  | $n, y, y$ | 1,1,1 | 1,2,2 |
| 8:20 AM | $y, y(D . O), y, y$ | $y$ | $y, n, n$ | 1, 1, 1, 1,1 | 2, 1, 1, 1, 1 |
| 8:25 AM | $y, y, y$ | $y$ |  | 1, 1, 1, 1 | 1, 1, 1, 1 |
| 8:30 AM |  |  |  |  |  |
| 8:35 AM | $y, y, y$ |  | y | 1, 1, 1 | 2, 1, 1 |
| 8:40 AM | $y, y$ | $y, y$ |  | 1,1,1,1 | 1,1,1,1 |
| 8:45 AM |  |  |  |  |  |
| 8:50 AM | $y, y, y, y$ |  |  | 1, 1, 1, 1 | 1, 1, 1, 1 |
| 8:55 AM |  | y, y | y, n | 1,1, | 2,1 |
| 9:00 AM | $y, y$ |  | n, y | 1,1 | 1,2 |



## Additional Notes: <br> D. $=$ Drop off <br> 1 motor vehicle <br> $y=y e s$ $n=n o$

Eventually, around 7:45 AM, the basketball court was transformed into more pickleball courts
Every Hour is based on the "Every 15 mins" calculation

## Methodology Overview

This form facilitates trip generation estimation using data within the Institute of Transportation Engineer's (ITE) Trip Generation Manual, 11th Edition and methodology described within ITE's Trip Generation Handbook, 3rd Edition. These references will be referred to as Manual and Handbook, respectively. The Manual contains data collected by various transportation professionals for a wide range of different land uses, with each land use category represented by a land use code (LUC). Average rates and equations have been established that correlate the relationship between an independent variable that describes the development size and generated trips for each categorized LUC in various settings and time periods. The Handbook indicates an established methodology for how to use data contained within the Manual when to use the fitted curve instead of the average rate and when to adjustments to the volume of trips are appropriate and how to do so. The methodology steps are represented visually in boxes in Figure 3.1. This worksheet applies calculations for each box if applicable.

Box 1 - Define Study Site Land Use Type\&Site Characteristics,
| Box 2 - Define Site Context | Box 3 - Define Analysis Objectives Trip Types\&Time Period The analyst is to pick an appropriate LUC(s) based on the subject's zoning/land use(s)future land use(s). The size of the land use(s) is described in reference to an independent variable(s) specific to (each) the land use (example: 1,000 square feet of building area is relatively common). Context assessment is to "simply determine whether the study sites is in a multimodal setting" and "could have persons accessing the site by walking, bicycling, or riding transit." This assessment is used in Box 4. The Manual separates data into 4 setting categories - Rural, General Urban/Suburban, Dense Multi-Urban Use and Center City Core. This worksheet uses the following abbreviations, respectively: R, G, D, and C. The Manual does not have data for all settings of all land use codes. The "General Urban/Suburban" setting is used by default.

This tool will focus on vehicular trips for a 24-hour period on a typical weekday as well as its AM peak hour and PM peak hour. Other time period(s) may be of interest.
Land Use Types and Size

| Proposed Use | Amount Units | ITE LUC | ITE Land Use Name |
| :---: | :---: | :---: | :---: |
| Single Family Attached | 101 Dwelling Units | 215 | Single-Family Attached Housing |

Box 4 - Is Study Site Multimodal?
Per the Handbook, "if the objective is to establish a local trip generation rate for a particular land use or study site, the simplified approach (Box 9) may be acceptable but the Box 5 through 8 approach is required if the study site is located in an infill setting, contains a mix of uses on-site, or is near significant transit service."

Box 5/Box 9 - Estimate Baseline Trips/Estimate Vehicular Trips (Determine Equation)
Vehicle trips are estimated using rates/equations applicable to each LUC. When the appropriate graph has a fitted curve, the Handbook has a process (Figure 4.2) to determine when to use it versus using the weighted average rate or collecting local data. The methodology requires for engineering judgement in some circumstances and permits engineering judgement to override or make adjustments when appropriate to best project (example 1: study site is expected to operate differently than data in the applicable land use code - such as restaurant that is closed in the morning or in the evening; example 2: LUC data in a localized area fails to be represented by the typically selected fitted curve/weighted average rate - a small shop/LUC 820 , AM peak hour is skewed by the high y-intercept).

Equation Type: Equation Used [Equated Rate] (Type Abbreviations: Weighted Average Rate ("WA"), Fitted Curve Type: Equation Used [Equated Rate]

| Proposed Use | ADT | AM Peak Hour | PM Peak Hour | Saturday |
| :---: | :---: | :---: | :---: | :---: |
| Single Family Attached | FC: $\mathrm{T}=7.62^{*} \mathrm{X}-50.48$ [7.12] | FC: $\mathrm{T}=0.52^{*} \mathrm{X}-5.7$ [0.46] | FC: T=0.6*X-3.93 [0.56] | WA: $T=X^{*} 0.57$ [0.57] |

Box 5/Box 9-Estimate Baseline Trips/Estimate Vehicular Trips (Apply Equations and in/out Distributions)

| Proposed Use | ADT |  |  |  | AM Peak Hour |  |  |  | PM Peak Hour |  |  |  | Saturday |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | \% In | In | Out | Total | \% In | In | Out | Total | \% In | In | Out | Total | \% In | In | Out | Total |
| Single Family Attached | 50\% | 360 | 360 | 720 | 31\% | 15 | 32 | 47 | 57\% | 32 | 25 | 57 | 48\% | 28 | 30 | 58 |


| Proposed Use | ADT |  |  | AM Peak Hour |  |  | PM Peak Hour |  |  | Saturday |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In | Out | Total | In | Out | Total | In | Out | Total | In | Out | Total |
| Single Family Attached | 360 | 360 | 720 | 15 | 32 | 47 | 32 | 25 | 57 | 28 | 30 | 58 |
| Totals | 360 | 360 | 720 | 15 | 32 | 47 | 32 | 25 | 57 | 28 | 30 | 58 |

Net New Trips. Pass-by trips and truck trips may be subtracted from the total external vehicle trips, if applicable/data available. Diverted link trips may also be separated, but are often (conservatively) grouped with primary trips.

Net New Trips

| Proposed Use | ADT |  |  | AM Peak Hour |  |  | PM Peak Hour |  |  | Saturday |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In | Out | Total | In | Out | Total | In | Out | Total | In | Out | Total |
| Single Family Attached | 360 | 360 | 720 | 15 | 32 | 47 | 32 | 25 | 57 | 28 | 30 | 58 |
| Totals | 360 | 360 | 720 | 15 | 32 | 47 | 32 | 25 | 57 | 28 | 30 | 58 |


|  | 4 |  | 7 |  |  |  | $\uparrow$ | 1 | $\checkmark$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | ¢ | ${ }^{*}$ | $\uparrow$ | F | \％ | 性 | 「 | ${ }_{7}$ | 4 4 | 「 |
| Traffic Volume（vph） | 35 | － | 71 | 2 | 13 | 94 | 689 | 70 | 7 | 675 | 27 |
| Future Volume（vph） | 35 | 6 | 71 | 2 | 13 | 94 | 689 | 70 | 7 | 675 | 27 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 3 | 8 | 7 | 4 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases | 8 |  | 4 |  | 4 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 3 | 8 | 7 | 4 | 4 | 1 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 7.0 | 5.0 | 7.0 | 7.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 10.0 | 36.6 | 10.0 | 34.6 | 34.6 | 11.4 | 27.1 | 27.1 | 11.4 | 22.1 | 22.1 |
| Total Split（s） | 15.0 | 25.0 | 15.0 | 25.0 | 25.0 | 20.0 | 50.0 | 50.0 | 20.0 | 50.0 | 50.0 |
| Total Split（\％） | 13．6\％ | 22．7\％ | 13．6\％ | 22．7\％ | 22．7\％ | 18．2\％ | 45．5\％ | 45．5\％ | 18．2\％ | 45．5\％ | 45．5\％ |
| Yellow Time（s） | 3.0 | 3.3 | 3.0 | 3.3 | 3.3 | 4.4 | 5.1 | 5.1 | 4.4 | 5.1 | 5.1 |
| All－Red Time（s） | 2.0 | 2.3 | 2.0 | 2.3 | 2.3 | 2.0 | 1.0 | 1.0 | 2.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 5.0 | 5.6 | 5.0 | 5.6 | 5.6 | 6.4 | 6.1 | 6.1 | 6.4 | 6.1 | 6.1 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C－Max | C－Max | None | C－Max | C－Max |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 110
Actuated Cycle Length： 110
Offset： 8 （7\％），Referenced to phase 2：SBTL and 6：NBTL，Start of Green
Natural Cycle： 90
Control Type：Actuated－Coordinated
Splits and Phases：1：Scottsdale Rd．\＆Ashler Hills Dr．


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{4}$ | 4 | 「 | ${ }^{7}$ | 中4 | F | ${ }^{7}$ | 中4 | 「 |
| Traffic Volume（veh／h） | 35 | 6 | 105 | 71 | 2 | 13 | 94 | 689 | 70 | 7 | 675 | 27 |
| Future Volume（veh／h） | 35 | 6 | 105 | 71 | 2 | 13 | 94 | 689 | 70 | 7 | 675 | 27 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 38 | 7 | 86 | 77 | 2 | 6 | 102 | 749 | 38 | 8 | 734 | 14 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 228 | 9 | 112 | 183 | 181 | 154 | 513 | 2317 | 1034 | 468 | 2198 | 980 |
| Arrive On Green | 0.03 | 0.08 | 0.08 | 0.05 | 0.10 | 0.10 | 0.04 | 0.65 | 0.65 | 0.01 | 0.62 | 0.62 |
| Sat Flow，veh／h | 1781 | 121 | 1483 | 1781 | 1870 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 38 | 0 | 93 | 77 | 2 | 6 | 102 | 749 | 38 | 8 | 734 | 14 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1603 | 1781 | 1870 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 2.1 | 0.0 | 6.3 | 4.3 | 0.1 | 0.4 | 2.3 | 10.2 | 0.9 | 0.2 | 10.9 | 0.4 |
| Cycle Q Clear（g＿c），s | 2.1 | 0.0 | 6.3 | 4.3 | 0.1 | 0.4 | 2.3 | 10.2 | 0.9 | 0.2 | 10.9 | 0.4 |
| Prop In Lane | 1.00 |  | 0.92 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 228 | 0 | 122 | 183 | 181 | 154 | 513 | 2317 | 1034 | 468 | 2198 | 980 |
| V／C Ratio（X） | 0.17 | 0.00 | 0.76 | 0.42 | 0.01 | 0.04 | 0.20 | 0.32 | 0.04 | 0.02 | 0.33 | 0.01 |
| Avail Cap（c＿a），veh／h | 334 | 0 | 283 | 252 | 330 | 280 | 656 | 2317 | 1034 | 670 | 2198 | 980 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 44.8 | 0.0 | 49.9 | 43.9 | 44.9 | 45.0 | 7.3 | 8.4 | 6.8 | 7.8 | 10.1 | 8.1 |
| Incr Delay（d2），s／veh | 0.1 | 0.0 | 3.7 | 0.6 | 0.0 | 0.0 | 0.1 | 0.4 | 0.1 | 0.0 | 0.4 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.0 | 0.0 | 2.6 | 1.9 | 0.0 | 0.2 | 0.8 | 3.8 | 0.3 | 0.1 | 4.2 | 0.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 44.9 | 0.0 | 53.6 | 44.5 | 44.9 | 45.1 | 7.4 | 8.8 | 6.9 | 7.8 | 10.5 | 8.1 |
| LnGrp LOS | D | A | D | D | D | D | A | A | A | A | B | A |
| Approach Vol，veh／h |  | 131 |  |  | 85 |  |  | 889 |  |  | 756 |  |
| Approach Delay，s／veh |  | 51.1 |  |  | 44.5 |  |  | 8.6 |  |  | 10.4 |  |
| Approach LOS |  | D |  |  | D |  |  | A |  |  | B |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 11.2 | 74.1 | 8.4 | 16.3 | 7.5 | 77.8 | 10.8 | 13.9 |
| Change Period（Y＋Rc），s | 6.4 | 6.1 | 5.0 | 5.6 | 6.4 | 6.1 | 5.0 | 5.6 |
| Max Green Setting（Gmax），s | 13.6 | 43.9 | 10.0 | 19.4 | 13.6 | 43.9 | 10.0 | 19.4 |
| Max Q Clear Time（g＿c＋11），s | 4.3 | 12.9 | 4.1 | 2.4 | 2.2 | 12.2 | 6.3 | 8.3 |
| Green Ext Time（p＿c），s | 0.1 | 3.7 | 0.0 | 0.0 | 0.0 | 3.9 | 0.0 | 0.2 |

## Intersection Summary

| HCM 6th Ctrl Delay | 14.0 |
| :--- | ---: |
| HCM 6th LOS | B |

## Notes

User approved pedestrian interval to be less than phase max green．

|  | 4 |  |  |  |  |  | $\uparrow$ | 1 | $\checkmark$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{F}$ | ${ }^{7}$ | $\uparrow$ | F＇ | ${ }^{*}$ | 性 | 「 | ${ }_{1}$ | 个4 | 「 |
| Traffic Volume（vph） | 18 | 8 | 250 | 13 | 28 | 39 | 936 | 116 | 21 | 712 | 10 |
| Future Volume（vph） | 18 | 8 | 250 | 13 | 28 | 39 | 936 | 116 | 21 | 712 | 10 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 3 | 8 | 7 | 4 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases | 8 |  | 4 |  | 4 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 3 | 8 | 7 | 4 | 4 | 1 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 7.0 | 5.0 | 7.0 | 7.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 10.0 | 36.6 | 10.0 | 34.6 | 34.6 | 11.4 | 27.1 | 27.1 | 11.4 | 22.1 | 22.1 |
| Total Split（s） | 15.0 | 25.0 | 15.0 | 25.0 | 25.0 | 20.0 | 50.0 | 50.0 | 20.0 | 50.0 | 50.0 |
| Total Split（\％） | 13．6\％ | 22．7\％ | 13．6\％ | 22．7\％ | 22．7\％ | 18．2\％ | 45．5\％ | 45．5\％ | 18．2\％ | 45．5\％ | 45．5\％ |
| Yellow Time（s） | 3.0 | 3.3 | 3.0 | 3.3 | 3.3 | 4.4 | 5.1 | 5.1 | 4.4 | 5.1 | 5.1 |
| All－Red Time（s） | 2.0 | 2.3 | 2.0 | 2.3 | 2.3 | 2.0 | 1.0 | 1.0 | 2.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 5.0 | 5.6 | 5.0 | 5.6 | 5.6 | 6.4 | 6.1 | 6.1 | 6.4 | 6.1 | 6.1 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C－Max | C－Max | None | C－Max | C－Max |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 110
Actuated Cycle Length： 110
Offset： 8 （7\％），Referenced to phase 2：SBTL and 6：NBTL，Start of Green
Natural Cycle： 90
Control Type：Actuated－Coordinated
Splits and Phases：1：Scottsdale Rd．\＆Ashler Hills Dr．


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | 44 | 「 | ${ }^{*}$ | 革 | 7 |
| Traffic Volume（veh／h） | 18 | 8 | 36 | 250 | 13 | 28 | 39 | 936 | 116 | 21 | 712 | 10 |
| Future Volume（veh／h） | 18 | 8 | 36 | 250 | 13 | 28 | 39 | 936 | 116 | 21 | 712 | 10 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 20 | 9 | 29 | 272 | 14 | 15 | 42 | 1017 | 63 | 23 | 774 | 6 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 184 | 23 | 74 | 278 | 242 | 205 | 469 | 2193 | 978 | 348 | 2157 | 962 |
| Arrive On Green | 0.02 | 0.06 | 0.06 | 0.09 | 0.13 | 0.13 | 0.03 | 0.62 | 0.62 | 0.02 | 0.61 | 0.61 |
| Sat Flow，veh／h | 1781 | 389 | 1255 | 1781 | 1870 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 20 | 0 | 38 | 272 | 14 | 15 | 42 | 1017 | 63 | 23 | 774 | 6 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1644 | 1781 | 1870 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 1.1 | 0.0 | 2.4 | 10.0 | 0.7 | 0.9 | 1.0 | 16.9 | 1.7 | 0.5 | 12.0 | 0.2 |
| Cycle Q Clear（g＿c），s | 1.1 | 0.0 | 2.4 | 10.0 | 0.7 | 0.9 | 1.0 | 16.9 | 1.7 | 0.5 | 12.0 | 0.2 |
| Prop In Lane | 1.00 |  | 0.76 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 184 | 0 | 97 | 278 | 242 | 205 | 469 | 2193 | 978 | 348 | 2157 | 962 |
| V／C Ratio（X） | 0.11 | 0.00 | 0.39 | 0.98 | 0.06 | 0.07 | 0.09 | 0.46 | 0.06 | 0.07 | 0.36 | 0.01 |
| Avail Cap（c＿a），veh／h | 309 | 0 | 290 | 278 | 330 | 280 | 630 | 2193 | 978 | 528 | 2157 | 962 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 47.1 | 0.0 | 49.8 | 46.6 | 42.0 | 42.1 | 8.0 | 11.3 | 8.4 | 8.8 | 10.9 | 8.5 |
| Incr Delay（d2），s／veh | 0.1 | 0.0 | 0.9 | 47.7 | 0.0 | 0.1 | 0.0 | 0.7 | 0.1 | 0.0 | 0.5 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.5 | 0.0 | 1.0 | 6.3 | 0.3 | 0.4 | 0.4 | 6.5 | 0.6 | 0.2 | 4.7 | 0.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 47.2 | 0.0 | 50.8 | 94.3 | 42.0 | 42.2 | 8.0 | 12.0 | 8.5 | 8.8 | 11.3 | 8.5 |
| LnGrp LOS | D | A | D | F | D | D | A | B | A | A | B | A |
| Approach Vol，veh／h |  | 58 |  |  | 301 |  |  | 1122 |  |  | 803 |  |
| Approach Delay，s／veh |  | 49.5 |  |  | 89.3 |  |  | 11.7 |  |  | 11.2 |  |
| Approach LOS |  | D |  |  | F |  |  | B |  |  | B |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 10.0 | 72.9 | 7.3 | 19.8 | 8.9 | 74.0 | 15.0 | 12.1 |
| Change Period（Y＋Rc），s | 6.4 | 6.1 | 5.0 | 5.6 | 6.4 | 6.1 | 5.0 | 5.6 |
| Max Green Setting（Gmax），s | 13.6 | 43.9 | 10.0 | 19.4 | 13.6 | 43.9 | 10.0 | 19.4 |
| Max Q Clear Time（g＿c＋I1），s | 3.0 | 14.0 | 3.1 | 2.9 | 2.5 | 18.9 | 12.0 | 4.4 |
| Green Ext Time（p＿c），s | 0.0 | 4.0 | 0.0 | 0.0 | 0.0 | 5.5 | 0.0 | 0.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 22.7 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

User approved pedestrian interval to be less than phase max green．

|  | 4 |  |  |  |  |  | 4 | 7 | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{\beta}$ | ${ }^{7}$ | $\uparrow$ | F | ${ }^{7}$ | 性 | F | ${ }^{7}$ | 个 $\uparrow$ | 「 |
| Traffic Volume（vph） | 13 | 8 | 236 | 13 | 32 | 57 | 938 | 160 | 35 | 787 | 12 |
| Future Volume（vph） | 13 | 8 | 236 | 13 | 32 | 57 | 938 | 160 | 35 | 787 | 12 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | ， | 8 | 7 | 4 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases | 8 |  | 4 |  | 4 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 3 | 8 | 7 | 4 | 4 | 1 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 7.0 | 5.0 | 7.0 | 7.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 10.0 | 36.6 | 10.0 | 34.6 | 34.6 | 11.4 | 27.1 | 27.1 | 11.4 | 22.1 | 22.1 |
| Total Split（s） | 15.0 | 25.0 | 15.0 | 25.0 | 25.0 | 20.0 | 50.0 | 50.0 | 20.0 | 50.0 | 50.0 |
| Total Split（\％） | 13．6\％ | 22．7\％ | 13．6\％ | 22．7\％ | 22．7\％ | 18．2\％ | 45．5\％ | 45．5\％ | 18．2\％ | 45．5\％ | 45．5\％ |
| Yellow Time（s） | 3.0 | 3.3 | 3.0 | 3.3 | 3.3 | 4.4 | 5.1 | 5.1 | 4.4 | 5.1 | 5.1 |
| All－Red Time（s） | 2.0 | 2.3 | 2.0 | 2.3 | 2.3 | 2.0 | 1.0 | 1.0 | 2.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 5.0 | 5.6 | 5.0 | 5.6 | 5.6 | 6.4 | 6.1 | 6.1 | 6.4 | 6.1 | 6.1 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C－Max | C－Max | None | C－Max | C－Max |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length： 110
Actuated Cycle Length： 110
Offset： 8 （7\％），Referenced to phase 2：SBTL and 6：NBTL，Start of Green
Natural Cycle： 90
Control Type：Actuated－Coordinated
Splits and Phases：1：Scottsdale Rd．\＆Ashler Hills Dr．


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | 44 | 「 | ${ }^{7}$ | 性 | 7 |
| Traffic Volume（veh／h） | 13 | 8 | 46 | 236 | 13 | 32 | 57 | 938 | 160 | 35 | 787 | 12 |
| Future Volume（veh／h） | 13 | 8 | 46 | 236 | 13 | 32 | 57 | 938 | 160 | 35 | 787 | 12 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 14 | 9 | 38 | 257 | 14 | 18 | 62 | 1020 | 87 | 38 | 855 | 6 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 176 | 19 | 79 | 271 | 253 | 214 | 439 | 2160 | 964 | 350 | 2134 | 952 |
| Arrive On Green | 0.02 | 0.06 | 0.06 | 0.09 | 0.14 | 0.14 | 0.04 | 0.61 | 0.61 | 0.03 | 0.60 | 0.60 |
| Sat Flow，veh／h | 1781 | 313 | 1320 | 1781 | 1870 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 14 | 0 | 47 | 257 | 14 | 18 | 62 | 1020 | 87 | 38 | 855 | 6 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1633 | 1781 | 1870 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 0.8 | 0.0 | 3.1 | 10.0 | 0.7 | 1.1 | 1.4 | 17.4 | 2.5 | 0.9 | 13.9 | 0.2 |
| Cycle Q Clear（g＿c），s | 0.8 | 0.0 | 3.1 | 10.0 | 0.7 | 1.1 | 1.4 | 17.4 | 2.5 | 0.9 | 13.9 | 0.2 |
| Prop In Lane | 1.00 |  | 0.81 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 176 | 0 | 98 | 271 | 253 | 214 | 439 | 2160 | 964 | 350 | 2134 | 952 |
| V／C Ratio（X） | 0.08 | 0.00 | 0.48 | 0.95 | 0.06 | 0.08 | 0.14 | 0.47 | 0.09 | 0.11 | 0.40 | 0.01 |
| Avail Cap（c＿a），veh／h | 310 | 0 | 288 | 271 | 330 | 280 | 590 | 2160 | 964 | 515 | 2134 | 952 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 47.4 | 0.0 | 50.0 | 46.1 | 41.5 | 41.6 | 8.4 | 11.9 | 8.9 | 9.0 | 11.6 | 8.8 |
| Incr Delay（d2），s／veh | 0.1 | 0.0 | 1.4 | 40.4 | 0.0 | 0.1 | 0.1 | 0.7 | 0.2 | 0.1 | 0.6 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.4 | 0.0 | 1.3 | 5.2 | 0.3 | 0.4 | 0.5 | 6.7 | 0.9 | 0.3 | 5.4 | 0.1 |

Unsig．Movement Delay，s／veh

| LnGrp Delay（d），s／veh | 47.4 | 0.0 | 51.4 | 86.5 | 41.5 | 41.7 | 8.4 | 12.6 | 9.1 | 9.0 | 12.1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | D | A | D | F | D | D | A | B | A | A | B |
| Approach Vol，veh／h |  | 61 |  |  | 289 |  | 1169 |  | 899 |  |  |
| Approach Delay，s／veh | 50.5 |  |  | 81.6 |  |  | 12.1 |  | 12.0 |  |  |
| Approach LOS | D |  |  | F |  |  | B |  |  |  |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 10.6 | 72.2 | 6.7 | 20.5 | 9.8 | 73.0 | 15.0 | 12.2 |
| Change Period（Y＋Rc），s | 6.4 | 6.1 | 5.0 | 5.6 | 6.4 | 6.1 | 5.0 | 5.6 |
| Max Green Setting（Gmax），s | 13.6 | 43.9 | 10.0 | 19.4 | 13.6 | 43.9 | 10.0 | 19.4 |
| Max Q Clear Time（g＿c＋I1），s | 3.4 | 15.9 | 2.8 | 3.1 | 2.9 | 19.4 | 12.0 | 5.1 |
| Green Ext Time（p＿c），s | 0.0 | 4.4 | 0.0 | 0.0 | 0.0 | 5.6 | 0.0 | 0.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 21.3 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

User approved pedestrian interval to be less than phase max green．

| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | $\hat{\square}$ | ${ }^{7}$ | $\uparrow$ | 「 | \％ | 个个 | 「 | ${ }^{1}$ | 个个 | 「 |
| Traffic Volume（vph） | 35 | 6 | 83 | 3 | 33 | 95 | 696 | 77 | 16 | 682 | 27 |
| Future Volume（vph） | 35 | 6 | 83 | 3 | 33 | 95 | 696 | 77 | 16 | 682 | 27 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 3 | 8 | 7 | 4 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases | 8 |  | 4 |  | 4 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 3 | 8 | 7 | 4 | 4 | 1 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 10.0 | 5.0 | 7.0 | 7.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 10.0 | 36.6 | 10.0 | 34.6 | 34.6 | 11.4 | 27.1 | 27.1 | 11.4 | 22.1 | 22.1 |
| Total Split（s） | 10.0 | 39.0 | 12.0 | 41.0 | 41.0 | 20.0 | 56.0 | 56.0 | 13.0 | 49.0 | 49.0 |
| Total Split（\％） | 8．3\％ | 32．5\％ | 10．0\％ | 34．2\％ | 34．2\％ | 16．7\％ | 46．7\％ | 46．7\％ | 10．8\％ | 40．8\％ | 40．8\％ |
| Yellow Time（s） | 3.0 | 3.3 | 3.0 | 3.3 | 3.3 | 4.4 | 5.1 | 5.1 | 4.4 | 5.1 | 5.1 |
| All－Red Time（s） | 2.0 | 2.3 | 2.0 | 2.3 | 2.3 | 2.0 | 1.0 | 1.0 | 2.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 5.0 | 5.6 | 5.0 | 5.6 | 5.6 | 6.4 | 6.1 | 6.1 | 6.4 | 6.1 | 6.1 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C－Max | C－Max | None | C－Max | C－Max |
| Act Efftt Green（s） | 15.9 | 10.3 | 20.9 | 16.1 | 16.1 | 84.4 | 81.6 | 81.6 | 78.0 | 73.2 | 73.2 |
| Actuated g／C Ratio | 0.13 | 0.09 | 0.17 | 0.13 | 0.13 | 0.70 | 0.68 | 0.68 | 0.65 | 0.61 | 0.61 |
| v／c Ratio | 0.19 | 0.51 | 0.47 | 0.01 | 0.10 | 0.22 | 0.31 | 0.08 | 0.04 | 0.34 | 0.03 |
| Control Delay | 42.7 | 18.6 | 50.3 | 48.3 | 0.5 | 6.4 | 9.0 | 0.6 | 5.6 | 12.3 | 0.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 42.7 | 18.6 | 50.3 | 48.3 | 0.5 | 6.4 | 9.0 | 0.6 | 5.6 | 12.3 | 0.0 |
| LOS | D | B | D | D | A | A | A | A | A | B | A |
| Approach Delay |  | 24.3 |  | 36.3 |  |  | 7.9 |  |  | 11.7 |  |
| Approach LOS |  | C |  | D |  |  | A |  |  | B |  |

## Intersection Summary

Cycle Length： 120
Actuated Cycle Length： 120
Offset： $8(7 \%)$ ，Referenced to phase $2:$ SBTL and 6 ：NBTL，Start of Green
Natural Cycle： 90
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.51
Intersection Signal Delay： 12.5 Intersection LOS：B

Intersection Capacity Utilization 50．5\％ ICU Level of Service A
Analysis Period（min） 15
Splits and Phases：1：Scottsdale Rd．\＆Ashler Hills Dr．


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | ${ }^{1}$ | 4 | 「 | ${ }^{7}$ | 44 | 「＇ | ${ }_{1}$ | 來 | 「 |
| Traffic Volume（veh／h） | 35 | 6 | 106 | 83 | 3 | 33 | 95 | 696 | 77 | 16 | 682 | 27 |
| Future Volume（veh／h） | 35 | 6 | 106 | 83 | 3 | 33 | 95 | 696 | 77 | 16 | 682 | 27 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 38 | 7 | 87 | 90 | 3 | 18 | 103 | 757 | 43 | 17 | 741 | 14 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 229 | 10 | 123 | 197 | 208 | 176 | 506 | 2304 | 1028 | 468 | 2225 | 992 |
| Arrive On Green | 0.03 | 0.08 | 0.08 | 0.06 | 0.11 | 0.11 | 0.04 | 0.65 | 0.65 | 0.02 | 0.63 | 0.63 |
| Sat Flow，veh／h | 1781 | 119 | 1484 | 1781 | 1870 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 38 | 0 | 94 | 90 | 3 | 18 | 103 | 757 | 43 | 17 | 741 | 14 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1603 | 1781 | 1870 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 2.3 | 0.0 | 6.9 | 5.5 | 0.2 | 1.2 | 2.5 | 11.4 | 1.2 | 0.4 | 11.8 | 0.4 |
| Cycle Q Clear（g＿c），s | 2.3 | 0.0 | 6.9 | 5.5 | 0.2 | 1.2 | 2.5 | 11.4 | 1.2 | 0.4 | 11.8 | 0.4 |
| Prop In Lane | 1.00 |  | 0.93 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 229 | 0 | 133 | 197 | 208 | 176 | 506 | 2304 | 1028 | 468 | 2225 | 992 |
| V／C Ratio（X） | 0.17 | 0.00 | 0.71 | 0.46 | 0.01 | 0.10 | 0.20 | 0.33 | 0.04 | 0.04 | 0.33 | 0.01 |
| Avail Cap（c＿a），veh／h | 249 | 0 | 446 | 197 | 552 | 468 | 636 | 2304 | 1028 | 534 | 2225 | 992 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 48.3 | 0.0 | 53.6 | 46.5 | 47.5 | 47.9 | 7.8 | 9.4 | 7.6 | 8.0 | 10.6 | 8.5 |
| Incr Delay（d2），s／veh | 0.1 | 0.0 | 2.6 | 0.6 | 0.0 | 0.1 | 0.1 | 0.4 | 0.1 | 0.0 | 0.4 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.0 | 0.0 | 2.9 | 2.5 | 0.1 | 0.5 | 0.9 | 4.4 | 0.4 | 0.2 | 4.6 | 0.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 48.4 | 0.0 | 56.2 | 47.1 | 47.5 | 48.0 | 7.8 | 9.8 | 7.7 | 8.0 | 11.0 | 8.5 |
| LnGrp LOS | D | A | E | D | D | D | A | A | A | A | B | A |
| Approach Vol，veh／h |  | 132 |  |  | 111 |  |  | 903 |  |  | 772 |  |
| Approach Delay，s／veh |  | 54.0 |  |  | 47.3 |  |  | 9.5 |  |  | 10.9 |  |
| Approach LOS |  | D |  |  | D |  |  | A |  |  | B |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 11.2 | 81.2 | 8.6 | 18.9 | 8.6 | 83.9 | 12.0 | 15.5 |
| Change Period（Y＋Rc），s | 6.4 | 6.1 | 5.0 | 5.6 | 6.4 | 6.1 | 5.0 | 5.6 |
| Max Green Setting（Gmax），s | 13.6 | 42.9 | 5.0 | 35.4 | 6.6 | 49.9 | 7.0 | 33.4 |
| Max Q Clear Time（g＿c＋I1），s | 4.5 | 13.8 | 4.3 | 3.2 | 2.4 | 13.4 | 7.5 | 8.9 |
| Green Ext Time（p＿c），s | 0.1 | 3.8 | 0.0 | 0.0 | 0.0 | 4.0 | 0.0 | 0.3 |

## Intersection Summary

| HCM 6th Ctrl Delay | 15.3 |
| :--- | ---: |
| HCM 6th LOS | B |

Notes
User approved pedestrian interval to be less than phase max green．

| Intersection |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0 |  |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |
| Lane Configurations | ${ }^{7}$ | 4 | $\uparrow$ |  | * |  |  |
| Traffic Vol, veh/h | 0 | 23 | 41 | 0 | 0 | 0 |  |
| Future Vol, veh/h | 0 | 23 | 41 | 0 | 0 | 0 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control F | Free | Free | Free | Free | Stop | Stop |  |
| RT Channelized | - | None | - | None | - | None |  |
| Storage Length | 75 | - | - | - | 0 | - |  |
| Veh in Median Storage, \# | \# | 0 | 0 | - | 0 | - |  |
| Grade, \% | - | 0 | 0 | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 0 | 25 | 45 | 0 | 0 | 0 |  |


| Major/Minor M | Major1 |  |  |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 45 | 0 | - | 0 | 70 | 45 |
| Stage 1 | - | - | - | - | 45 | - |
| Stage 2 | - | - | - | - | 25 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1563 | - | - | - | 934 | 1025 |
| Stage 1 | - | - | - | - | 977 | - |
| Stage 2 | - | - | - | - | 998 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1563 | - | - | - | 934 | 1025 |
| Mov Cap-2 Maneuver | - | - | - | - | 934 | - |
| Stage 1 | - | - | - | - | 977 | - |
| Stage 2 | - | - | - | - | 998 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  |  |  | SB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 0 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | BT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1563 | - | - | - | - |
| HCM Lane V/C Ratio |  | - | - | - | - | - |
| HCM Control Delay (s) |  | 0 | - | - | - | 0 |
| HCM Lane LOS |  | A | - | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | - |


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\hat{F}$ | \％ | $\uparrow$ | 「 | ${ }^{7}$ | 个4 | 「 | ${ }_{1}$ | 个个 | 「 |
| Traffic Volume（vph） | 18 | 9 | 262 | 14 | 44 | 39 | 945 | 128 | 41 | 719 | 10 |
| Future Volume（vph） | 18 | 9 | 262 | 14 | 44 | 39 | 945 | 128 | 41 | 719 | 10 |
| Turn Type | pm＋pt | NA | $\mathrm{pm}+\mathrm{pt}$ | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 3 | 8 | 7 | 4 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases | 8 |  | 4 |  | 4 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 3 | 8 | 7 | 4 | 4 | 1 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 10.0 | 5.0 | 7.0 | 7.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 10.0 | 36.6 | 10.0 | 34.6 | 34.6 | 11.4 | 27.1 | 27.1 | 11.4 | 22.1 | 22.1 |
| Total Split（s） | 14.4 | 36.6 | 22.4 | 44.6 | 44.6 | 11.4 | 49.0 | 49.0 | 12.0 | 49.6 | 49.6 |
| Total Split（\％） | 12．0\％ | 30．5\％ | 18．7\％ | 37．2\％ | 37．2\％ | 9．5\％ | 40．8\％ | 40．8\％ | 10．0\％ | 41．3\％ | 41．3\％ |
| Yellow Time（s） | 3.0 | 3.3 | 3.0 | 3.3 | 3.3 | 4.4 | 5.1 | 5.1 | 4.4 | 5.1 | 5.1 |
| All－Red Time（s） | 2.0 | 2.3 | 2.0 | 2.3 | 2.3 | 2.0 | 1.0 | 1.0 | 2.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 5.0 | 5.6 | 5.0 | 5.6 | 5.6 | 6.4 | 6.1 | 6.1 | 6.4 | 6.1 | 6.1 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C－Max | C－Max | None | C－Max | C－Max |
| Act Efft Green（s） | 14.2 | 10.0 | 29.6 | 24.4 | 24.4 | 73.8 | 69.4 | 69.4 | 74.0 | 69.5 | 69.5 |
| Actuated g／C Ratio | 0.12 | 0.08 | 0.25 | 0.20 | 0.20 | 0.62 | 0.58 | 0.58 | 0.62 | 0.58 | 0.58 |
| v／c Ratio | 0.11 | 0.28 | 0.82 | 0.04 | 0.11 | 0.10 | 0.50 | 0.14 | 0.15 | 0.38 | 0.01 |
| Control Delay | 34.5 | 25.1 | 60.1 | 39.9 | 0.5 | 9.2 | 17.8 | 1.3 | 9.8 | 15.9 | 0.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.5 | 25.1 | 60.1 | 39.9 | 0.5 | 9.2 | 17.8 | 1.3 | 9.8 | 15.9 | 0.0 |
| LOS | C | C | E | D | A | A | B | A | A | B | A |
| Approach Delay |  | 27.8 |  | 51.0 |  |  | 15.6 |  |  | 15.4 |  |
| Approach LOS |  | C |  | D |  |  | B |  |  | B |  |

## Intersection Summary

Cycle Length： 120
Actuated Cycle Length： 120
Offset： 0 （ $0 \%$ ），Referenced to phase 2：SBTL and 6：NBTL，Start of Green
Natural Cycle： 90
Control Type：Actuated－Coordinated
Maximum v／c Ratio： 0.82
Intersection Signal Delay： 20.9 Intersection LOS：C

Intersection Capacity Utilization 65．0\％
ICU Level of Service C
Analysis Period（min） 15
Splits and Phases：1：Scottsdale Rd．\＆Ashler Hills Dr．


| Intersection |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0 |  |  |  |  |  |  |
| Movement E | EBL | EBT | WBT | WBR | SBL |  |  |
| Lane Configurations | ${ }^{*}$ | 4 | F |  | * |  |  |
| Traffic Vol, veh/h | 0 | 56 | 46 | 0 | 0 | 0 |  |
| Future Vol, veh/h | 0 | 56 | 46 | 0 | 0 | 0 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control Fr | Free | Free | Free | Free | Stop | Stop |  |
| RT Channelized | - | None | - | None | - | None |  |
| Storage Length | 75 | - | - | - | 0 | - |  |
| Veh in Median Storage, \# | \# | 0 | 0 | - | 0 | - |  |
| Grade, \% | - | 0 | 0 | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 0 | 61 | 50 | 0 | 0 | 0 |  |


| Major/Minor M | Major1 |  |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 50 | 0 | 0 | 111 | 50 |
| Stage 1 | - | - | - | 50 | - |
| Stage 2 | - | - | - | 61 | - |
| Critical Hdwy | 4.12 | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1557 | - | - | 886 | 1018 |
| Stage 1 | - | - | - | 972 | - |
| Stage 2 | - | - | - | 962 | - |
| Platoon blocked, \% |  | - | - |  |  |
| Mov Cap-1 Maneuver | 1557 | - | - | 886 | 1018 |
| Mov Cap-2 Maneuver | - | - | - | 886 | - |
| Stage 1 | - | - | - | 972 | - |
| Stage 2 | - | - | - | 962 | - |
|  |  |  |  |  |  |
| Approach | EB |  |  | SB |  |
| HCM Control Delay, s | 0 |  |  | 0 |  |
| HCM LOS |  |  |  | A |  |
|  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1557 | - | - | - |
| HCM Lane V/C Ratio |  | - | - | - | - |
| HCM Control Delay (s) |  | 0 | - | - | 0 |
| HCM Lane LOS |  | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - |


|  | $\psi$ |  | $\%$ |  | $4$ | $4$ | $\dagger$ | \％ | $1$ | $\downarrow$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ | ${ }^{*}$ | 4 | 「 | ${ }^{*}$ | 中4 | 「 | ${ }^{*}$ | 中4 | F |
| Traffic Volume（vph） | 13 | 9 | 249 | 14 | 51 | 58 | 947 | 172 | 53 | 795 | 12 |
| Future Volume（vph） | 13 | 9 | 249 | 14 | 51 | 58 | 947 | 172 | 53 | 795 | 12 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 3 | 8 | 7 | 4 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases | 8 |  | 4 |  | 4 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 3 | 8 | 7 | 4 | 4 | 1 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 10.0 | 5.0 | 7.0 | 7.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 10.0 | 36.6 | 10.0 | 34.6 | 34.6 | 11.4 | 27.1 | 27.1 | 11.4 | 22.1 | 22.1 |
| Total Split（s） | 18.0 | 41.4 | 22.0 | 45.4 | 45.4 | 12.2 | 44.0 | 44.0 | 12.6 | 44.4 | 44.4 |
| Total Split（\％） | 15．0\％ | 34．5\％ | 18．3\％ | 37．8\％ | 37．8\％ | 10．2\％ | 36．7\％ | 36．7\％ | 10．5\％ | 37．0\％ | 37．0\％ |
| Yellow Time（s） | 3.0 | 3.3 | 3.0 | 3.3 | 3.3 | 4.4 | 5.1 | 5.1 | 4.4 | 5.1 | 5.1 |
| All－Red Time（s） | 2.0 | 2.3 | 2.0 | 2.3 | 2.3 | 2.0 | 1.0 | 1.0 | 2.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 5.0 | 5.6 | 5.0 | 5.6 | 5.6 | 6.4 | 6.1 | 6.1 | 6.4 | 6.1 | 6.1 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C－Max | C－Max | None | C－Max | C－Max |
| Act Effct Green（s） | 14.0 | 10.0 | 29.1 | 24.1 | 24.1 | 74.5 | 69.6 | 69.6 | 74.2 | 69.5 | 69.5 |
| Actuated g／C Ratio | 0.12 | 0.08 | 0.24 | 0.20 | 0.20 | 0.62 | 0.58 | 0.58 | 0.62 | 0.58 | 0.58 |
| v／c Ratio | 0.08 | 0.33 | 0.80 | 0.04 | 0.13 | 0.17 | 0.50 | 0.19 | 0.19 | 0.42 | 0.01 |
| Control Delay | 34.3 | 23.2 | 58.4 | 39.9 | 0.6 | 9.5 | 17.8 | 5.7 | 10.0 | 16.6 | 0.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.3 | 23.2 | 58.4 | 39.9 | 0.6 | 9.5 | 17.8 | 5.7 | 10.0 | 16.6 | 0.0 |
| LOS | C | C | E | D | A | A | B | A | A | B | A |
| Approach Delay |  | 25.3 |  | 48.3 |  |  | 15.6 |  |  | 15.9 |  |
| Approach LOS |  | C |  | D |  |  | B |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |
| Offset： $0(0 \%)$ ，Referenced to phase 2：SBTL and 6：NBTL，Start of Green |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 90 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 0.80 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 20.2 |  |  |  | Intersection LOS：C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 65．9\％ |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：1：Scottsdale Rd．\＆Ashler Hills Dr．


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | ${ }^{1}$ | 4 | 「＇ | ${ }^{7}$ | 44 | 「 | ${ }^{1}$ | 种 | 「 |
| Traffic Volume（veh／h） | 13 | 9 | 46 | 249 | 14 | 51 | 58 | 947 | 172 | 53 | 795 | 12 |
| Future Volume（veh／h） | 13 | 9 | 46 | 249 | 14 | 51 | 58 | 947 | 172 | 53 | 795 | 12 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 14 | 10 | 38 | 271 | 15 | 27 | 63 | 1029 | 95 | 58 | 864 | 6 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 198 | 28 | 105 | 384 | 387 | 328 | 382 | 1953 | 871 | 307 | 1949 | 869 |
| Arrive On Green | 0.02 | 0.08 | 0.08 | 0.14 | 0.21 | 0.21 | 0.04 | 0.55 | 0.55 | 0.04 | 0.55 | 0.55 |
| Sat Flow，veh／h | 1781 | 341 | 1296 | 1781 | 1870 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 14 | 0 | 48 | 271 | 15 | 27 | 63 | 1029 | 95 | 58 | 864 | 6 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1637 | 1781 | 1870 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 0.9 | 0.0 | 3.3 | 16.4 | 0.8 | 1.6 | 1.8 | 22.0 | 3.4 | 1.7 | 17.4 | 0.2 |
| Cycle Q Clear（g＿c），s | 0.9 | 0.0 | 3.3 | 16.4 | 0.8 | 1.6 | 1.8 | 22.0 | 3.4 | 1.7 | 17.4 | 0.2 |
| Prop In Lane | 1.00 |  | 0.79 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 198 | 0 | 132 | 384 | 387 | 328 | 382 | 1953 | 871 | 307 | 1949 | 869 |
| V／C Ratio（X） | 0.07 | 0.00 | 0.36 | 0.71 | 0.04 | 0.08 | 0.16 | 0.53 | 0.11 | 0.19 | 0.44 | 0.01 |
| Avail Cap（c＿a），veh／h | 363 | 0 | 488 | 384 | 620 | 526 | 403 | 1953 | 871 | 335 | 1949 | 869 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 49.4 | 0.0 | 52.2 | 41.1 | 38.0 | 38.4 | 12.1 | 17.1 | 13.0 | 13.0 | 16.2 | 12.3 |
| Incr Delay（d2），s／veh | 0.1 | 0.0 | 0.6 | 4.9 | 0.0 | 0.0 | 0.1 | 1.0 | 0.3 | 0.1 | 0.7 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.4 | 0.0 | 1.4 | 7.7 | 0.4 | 0.6 | 0.7 | 9.1 | 1.3 | 0.7 | 7.1 | 0.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 49.4 | 0.0 | 52.9 | 46.1 | 38.1 | 38.4 | 12.2 | 18.2 | 13.2 | 13.1 | 16.9 | 12.3 |
| LnGrp LOS | D | A | D | D | D | D | B | B | B | B | B | B |
| Approach Vol，veh／h |  | 62 |  |  | 313 |  |  | 1187 |  |  | 928 |  |
| Approach Delay，s／veh |  | 52.1 |  |  | 45.0 |  |  | 17.5 |  |  | 16.6 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | B |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 10.8 | 71.9 | 6.9 | 30.4 | 10.7 | 72.0 | 22.0 | 15.3 |
| Change Period（Y＋Rc），s | 6.4 | 6.1 | 5.0 | 5.6 | 6.4 | 6.1 | 5.0 | 5.6 |
| Max Green Setting（Gmax），s | 5.8 | 38.3 | 13.0 | 39.8 | 6.2 | 37.9 | 17.0 | 35.8 |
| Max Q Clear Time（g＿c＋I1），s | 3.8 | 19.4 | 2.9 | 3.6 | 3.7 | 24.0 | 18.4 | 5.3 |
| Green Ext Time（p＿c），s | 0.0 | 4.1 | 0.0 | 0.1 | 0.0 | 4.6 | 0.0 | 0.1 |

Intersection Summary

| HCM 6th Ctrl Delay | 21.5 |
| :--- | ---: |
| HCM 6th LOS | C |

Notes
User approved pedestrian interval to be less than phase max green．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | 1 | 个 | $\mathbf{F}$ |  | Mr |  |
| Traffic Vol, veh/h | 0 | 63 | 50 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 63 | 50 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 75 | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 68 | 54 | 0 | 0 | 0 |




|  | 4 | $\rightarrow$ | $\geqslant$ | $\dagger$ |  | 4 | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{1}$ |  | ${ }^{*}$ | 4 | 「 | \％ | 个4 | ＂ | ${ }_{1}$ | 个4 | F |
| Traffic Volume（veh／h） | 35 | 7 | 106 | 89 | 3 | 41 | 95 | 696 | 95 | 41 | 682 | 27 |
| Future Volume（veh／h） | 35 | 7 | 106 | 89 | 3 | 41 | 95 | 696 | 95 | 41 | 682 | 27 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 38 | 8 | 87 | 97 |  | 27 | 103 | 757 | 62 | 45 | 741 | 14 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 228 | 11 | 122 | 197 | 208 | 177 | 506 | 2252 | 1005 | 475 | 2224 | 992 |
| Arrive On Green | 0.03 | 0.08 | 0.08 | 0.06 | 0.11 | 0.11 | 0.04 | 0.63 | 0.63 | 0.03 | 0.63 | 0.63 |
| Sat Flow，veh／h | 1781 | 135 | 1470 | 1781 | 1870 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 38 | 0 | 95 | 97 | 3 | 27 | 103 | 757 | 62 | 45 | 741 | 14 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1606 | 1781 | 1870 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 2.3 | 0.0 | 6.9 | 5.9 | 0.2 | 1.8 | 2.5 | 11.9 | 1.8 | 1.1 | 11.8 | 0.4 |
| Cycle Q Clear（g＿c），s | 2.3 | 0.0 | 6.9 | 5.9 | 0.2 | 1.8 | 2.5 | 11.9 | 1.8 | 1.1 | 11.8 | 0.4 |
| Prop In Lane | 1.00 |  | 0.92 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 228 | 0 | 133 | 197 | 208 | 177 | 506 | 2252 | 1005 | 475 | 2224 | 992 |
| V／C Ratio（X） | 0.17 | 0.00 | 0.71 | 0.49 | 0.01 | 0.15 | 0.20 | 0.34 | 0.06 | 0.09 | 0.33 | 0.01 |
| Avail Cap（c＿a），veh／h | 249 | 0 | 447 | 197 | 552 | 468 | 636 | 2252 | 1005 | 515 | 2224 | 992 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 48.2 | 0.0 | 53.6 | 46.7 | 47.5 | 48.2 | 7.8 | 10.2 | 8.4 | 7.7 | 10.6 | 8.5 |
| Incr Delay（d2），s／veh | 0.1 | 0.0 | 2.6 | 0.7 | 0.0 | 0.1 | 0.1 | 0.4 | 0.1 | 0.0 | 0.4 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％oile BackOfQ（50\％），veh／ln | 1.0 | 0.0 | 2.9 | 2.7 | 0.1 | 0.7 | 0.9 | 4.6 | 0.6 | 0.4 | 4.6 | 0.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 48.4 | 0.0 | 56.3 | 47.4 | 47.5 | 48.3 | 7.9 | 10.6 | 8.5 | 7.8 | 11.0 | 8.5 |
| LnGrp LOS | D | A | E | D | D | D | A | B | A | A | B | A |
| Approach Vol，veh／h |  | 133 |  |  | 127 |  |  | 922 |  |  | 800 |  |
| Approach Delay，s／veh |  | 54.0 |  |  | 47.6 |  |  | 10.2 |  |  | 10.8 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | B |  |


|  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration $(G+Y+R c)$ ，s | 11.2 | 81.2 | 8.6 | 19.0 | 10.3 | 82.2 | 12.0 | 15.6 |
| Change Period $(\mathrm{Y}+\mathrm{Rc})$ ，s | 6.4 | 6.1 | 5.0 | 5.6 | 6.4 | 6.1 | 5.0 | 5.6 |
| Max Green Setting（Gmax），s | 13.6 | 42.9 | 5.0 | 35.4 | 6.6 | 49.9 | 7.0 | 33.4 |
| Max Q Clear Time（g＿c＋1）），s | 4.5 | 13.8 | 4.3 | 3.8 | 3.1 | 13.9 | 7.9 | 8.9 |
| Green Ext Time（p＿c），s | 0.1 | 3.8 | 0.0 | 0.0 | 0.0 | 4.0 | 0.0 | 0.3 |

## Intersection Summary

| HCM 6th Ctrl Delay | 15.8 |
| :--- | ---: |
| HCM 6th LOS | $B$ |

## Notes

User approved pedestrian interval to be less than phase max green．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.6 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | i | P | $\mathbf{F}$ |  | Mr |  |
| Traffic Vol, veh/h | 44 | 23 | 41 | 2 | 0 | 14 |
| Future Vol, veh/h | 44 | 23 | 41 | 2 | 0 | 14 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 75 | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 48 | 25 | 45 | 2 | 0 | 15 |



|  | 4 |  |  |  |  | 4 | $\uparrow$ |  |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ | \％ | $\uparrow$ | 「 | \％ | 个4 | 「 | \％ | 个4 | F |
| Traffic Volume（vph） | 18 | 10 | 271 | 15 | 56 | 39 | 945 | 138 | 54 | 719 | 10 |
| Future Volume（vph） | 18 | 10 | 271 | 15 | 56 | 39 | 945 | 138 | 54 | 719 | 10 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 3 | 8 | 7 | 4 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases | 8 |  | 4 |  | 4 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 3 | 8 | 7 | 4 | 4 | 1 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 10.0 | 5.0 | 7.0 | 7.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 10.0 | 36.6 | 10.0 | 34.6 | 34.6 | 11.4 | 27.1 | 27.1 | 11.4 | 22.1 | 22.1 |
| Total Split（s） | 14.4 | 36.6 | 22.4 | 44.6 | 44.6 | 11.4 | 49.0 | 49.0 | 12.0 | 49.6 | 49.6 |
| Total Split（\％） | 12．0\％ | 30．5\％ | 18．7\％ | 37．2\％ | 37．2\％ | 9．5\％ | 40．8\％ | 40．8\％ | 10．0\％ | 41．3\％ | 41．3\％ |
| Yellow Time（s） | 3.0 | 3.3 | 3.0 | 3.3 | 3.3 | 4.4 | 5.1 | 5.1 | 4.4 | 5.1 | 5.1 |
| All－Red Time（s） | 2.0 | 2.3 | 2.0 | 2.3 | 2.3 | 2.0 | 1.0 | 1.0 | 2.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 5.0 | 5.6 | 5.0 | 5.6 | 5.6 | 6.4 | 6.1 | 6.1 | 6.4 | 6.1 | 6.1 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C－Max | C－Max | None | C－Max | C－Max |
| Act Effct Green（s） | 14.2 | 10.0 | 29.7 | 24.5 | 24.5 | 73.3 | 69.0 | 69.0 | 74.2 | 69.4 | 69.4 |
| Actuated g／C Ratio | 0.12 | 0.08 | 0.25 | 0.20 | 0.20 | 0.61 | 0.58 | 0.58 | 0.62 | 0.58 | 0.58 |
| V／c Ratio | 0.11 | 0.29 | 0.85 | 0.04 | 0.14 | 0.10 | 0.50 | 0.15 | 0.19 | 0.38 | 0.01 |
| Control Delay | 34.5 | 25.6 | 62.9 | 40.0 | 0.7 | 9.3 | 18.1 | 1.8 | 10.1 | 15.9 | 0.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.5 | 25.6 | 62.9 | 40.0 | 0.7 | 9.3 | 18.1 | 1.8 | 10.1 | 15.9 | 0.0 |
| LOS | C | C | E | D | A | A | B | A | B | B | A |
| Approach Delay |  | 28.2 |  | 51.8 |  |  | 15.8 |  |  | 15.3 |  |
| Approach LOS |  | C |  | D |  |  | B |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |
| Offset： $0(0 \%)$ ，Referenced to phase 2：SBTL and 6：NBTL，Start of Green |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 90 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 0.85 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 21.3 |  |  |  | Intersection LOS：C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 67．1\％ |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：1：Scottsdale Rd．\＆Ashler Hills Dr．


|  | 4 |  |  | 7 |  | 4 | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\hat{\beta}$ |  | \％ | $\uparrow$ | 「 | ${ }^{7}$ | 个个 | 「 | ${ }^{4}$ | 州 | F |
| Traffic Volume（veh／h） | 18 | 10 | 36 | 271 | 15 | 56 | 39 | 945 | 138 | 54 | 719 | 10 |
| Future Volume（veh／h） | 18 | 10 | 36 | 271 | 15 | 56 | 39 | 945 | 138 | 54 | 719 | 10 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 20 | 11 | 29 | 295 | 16 | 37 | 42 | 1027 | 80 | 59 | 782 | 6 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 206 | 37 | 98 | 398 | 386 | 327 | 406 | 1938 | 864 | 307 | 1953 | 871 |
| Arrive On Green | 0.02 | 0.08 | 0.08 | 0.14 | 0.21 | 0.21 | 0.03 | 0.55 | 0.55 | 0.04 | 0.55 | 0.55 |
| Sat Flow，veh／h | 1781 | 455 | 1199 | 1781 | 1870 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 20 | 0 | 40 | 295 | 16 | 37 | 42 | 1027 | 80 | 59 | 782 | 6 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1654 | 1781 | 1870 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 1.2 | 0.0 | 2.7 | 17.4 | 0.8 | 2.3 | 1.2 | 22.2 | 2.9 | 1.7 | 15.2 | 0.2 |
| Cycle Q Clear（g＿c），s | 1.2 | 0.0 | 2.7 | 17.4 | 0.8 | 2.3 | 1.2 | 22.2 | 2.9 | 1.7 | 15.2 | 0.2 |
| Prop In Lane | 1.00 |  | 0.73 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 206 | 0 | 135 | 398 | 386 | 327 | 406 | 1938 | 864 | 307 | 1953 | 871 |
| V／C Ratio（X） | 0.10 | 0.00 | 0.30 | 0.74 | 0.04 | 0.11 | 0.10 | 0.53 | 0.09 | 0.19 | 0.40 | 0.01 |
| Avail Cap（c＿a），veh／h | 310 | 0 | 427 | 398 | 608 | 515 | 425 | 1938 | 864 | 327 | 1953 | 871 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 49.0 | 0.0 | 51.9 | 41.5 | 38.1 | 38.7 | 12.0 | 17.5 | 13.1 | 13.2 | 15.6 | 12.2 |
| Incr Delay（d2），s／veh | 0.1 | 0.0 | 0.5 | 6.4 | 0.0 | 0.1 | 0.0 | 1.0 | 0.2 | 0.1 | 0.6 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 0.6 | 0.0 | 1.2 | 8.6 | 0.4 | 0.9 | 0.5 | 9.1 | 1.1 | 0.7 | 6.2 | 0.1 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 49.0 | 0.0 | 52.3 | 47.9 | 38.2 | 38.8 | 12.0 | 18.5 | 13.3 | 13.3 | 16.2 | 12.2 |
| LnGrp LOS | D | A | D | D | D | D | B | B | B | B | B | B |
| Approach Vol，veh／h |  | 60 |  |  | 348 |  |  | 1149 |  |  | 847 |  |
| Approach Delay，s／veh |  | 51.2 |  |  | 46.4 |  |  | 17.9 |  |  | 16.0 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | B |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ）， s | 10.2 | 72.1 | 7.4 | 30.3 | 10.7 | 71.5 | 22.4 | 15.4 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ）， s | 6.4 | 6.1 | 5.0 | 5.6 | 6.4 | 6.1 | 5.0 | 5.6 |  |  |  |  |
| Max Green Setting（Gmax），s | 5.0 | 43.5 | 9.4 | 39.0 | 5.6 | 42.9 | 17.4 | 31.0 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 3.2 | 17.2 | 3.2 | 4.3 | 3.7 | 24.2 | 19.4 | 4.7 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 3.9 | 0.0 | 0.1 | 0.0 | 5.2 | 0.0 | 0.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 22.2 |  |  |  |  |  |  |  |  |  |
|  |  |  | C |  |  |  |  |  |  |  |  |  |

## Notes

User approved pedestrian interval to be less than phase max green．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | a | P | $\mathbf{F}$ |  | Mr |  |
| Traffic Vol, veh/h | 24 | 56 | 46 | 0 | 0 | 22 |
| Future Vol, veh/h | 24 | 56 | 46 | 0 | 0 | 22 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 75 | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 26 | 61 | 50 | 0 | 0 | 24 |



|  | 4 |  |  |  |  |  | $\uparrow$ |  |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\hat{\dagger}$ | \％ | 4 | 「 | \％ | 个4 | 「 | \％ | 个4 | F＇ |
| Traffic Volume（vph） | 13 | 10 | 256 | 15 | 61 | 58 | 947 | 192 | 80 | 795 | 12 |
| Future Volume（vph） | 13 | 10 | 256 | 15 | 61 | 58 | 947 | 192 | 80 | 795 | 12 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 3 | 8 | 7 | 4 |  | 1 | 6 |  | 5 | 2 |  |
| Permitted Phases | 8 |  | 4 |  | 4 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 3 | 8 | 7 | 4 | 4 | 1 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 5.0 | 10.0 | 5.0 | 7.0 | 7.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split（s） | 10.0 | 36.6 | 10.0 | 34.6 | 34.6 | 11.4 | 27.1 | 27.1 | 11.4 | 22.1 | 22.1 |
| Total Split（s） | 18.0 | 41.4 | 22.0 | 45.4 | 45.4 | 12.2 | 44.0 | 44.0 | 12.6 | 44.4 | 44.4 |
| Total Split（\％） | 15．0\％ | 34．5\％ | 18．3\％ | 37．8\％ | 37．8\％ | 10．2\％ | 36．7\％ | 36．7\％ | 10．5\％ | 37．0\％ | 37．0\％ |
| Yellow Time（s） | 3.0 | 3.3 | 3.0 | 3.3 | 3.3 | 4.4 | 5.1 | 5.1 | 4.4 | 5.1 | 5.1 |
| All－Red Time（s） | 2.0 | 2.3 | 2.0 | 2.3 | 2.3 | 2.0 | 1.0 | 1.0 | 2.0 | 1.0 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 5.0 | 5.6 | 5.0 | 5.6 | 5.6 | 6.4 | 6.1 | 6.1 | 6.4 | 6.1 | 6.1 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C－Max | C－Max | None | C－Max | C－Max |
| Act Effct Green（s） | 14.0 | 10.0 | 29.2 | 24.2 | 24.2 | 72.4 | 66.5 | 66.5 | 74.9 | 69.4 | 69.4 |
| Actuated g／C Ratio | 0.12 | 0.08 | 0.24 | 0.20 | 0.20 | 0.60 | 0.55 | 0.55 | 0.62 | 0.58 | 0.58 |
| V／c Ratio | 0.08 | 0.34 | 0.82 | 0.04 | 0.16 | 0.17 | 0.52 | 0.22 | 0.29 | 0.42 | 0.01 |
| Control Delay | 34.3 | 23.7 | 60.2 | 40.0 | 0.8 | 9.6 | 19.1 | 6.9 | 10.9 | 16.6 | 0.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.3 | 23.7 | 60.2 | 40.0 | 0.8 | 9.6 | 19.1 | 6.9 | 10.9 | 16.6 | 0.0 |
| LOS | C | C | E | D | A | A | B | A | B | B | A |
| Approach Delay |  | 25.7 |  | 48.4 |  |  | 16.7 |  |  | 15.9 |  |
| Approach LOS |  | C |  | D |  |  | B |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length： 120 |  |  |  |  |  |  |  |  |  |  |  |
| Offset： $0(0 \%)$ ，Referenced to phase 2：SBTL and 6：NBTL，Start of Green |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle： 90 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type：Actuated－Coordinated |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 0.82 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay： 20.9 |  |  |  | Intersection LOS：C |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 66．5\％ |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |
| Analysis Period（min） 15 |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases：1：Scottsdale Rd．\＆Ashler Hills Dr．


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | 「＇ | ${ }^{7}$ | 中4 | 「 | ${ }^{1}$ | 44 | 「 |
| Traffic Volume（veh／h） | 13 | 10 | 46 | 256 | 15 | 61 | 58 | 947 | 192 | 80 | 795 | 12 |
| Future Volume（veh／h） | 13 | 10 | 46 | 256 | 15 | 61 | 58 | 947 | 192 | 80 | 795 | 12 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate，veh／h | 14 | 11 | 38 | 278 | 16 | 38 | 63 | 1029 | 117 | 87 | 864 | 6 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap，veh／h | 198 | 30 | 104 | 385 | 389 | 329 | 381 | 1936 | 864 | 306 | 1946 | 868 |
| Arrive On Green | 0.02 | 0.08 | 0.08 | 0.14 | 0.21 | 0.21 | 0.04 | 0.54 | 0.54 | 0.04 | 0.55 | 0.55 |
| Sat Flow，veh／h | 1781 | 368 | 1273 | 1781 | 1870 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume（v），veh／h | 14 | 0 | 49 | 278 | 16 | 38 | 63 | 1029 | 117 | 87 | 864 | 6 |
| Grp Sat Flow（s），veh／h／ln | 1781 | 0 | 1641 | 1781 | 1870 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve（g＿s），s | 0.9 | 0.0 | 3.4 | 16.9 | 0.8 | 2.3 | 1.8 | 22.3 | 4.4 | 2.6 | 17.4 | 0.2 |
| Cycle Q Clear（g＿c），s | 0.9 | 0.0 | 3.4 | 16.9 | 0.8 | 2.3 | 1.8 | 22.3 | 4.4 | 2.6 | 17.4 | 0.2 |
| Prop In Lane | 1.00 |  | 0.78 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 198 | 0 | 134 | 385 | 389 | 329 | 381 | 1936 | 864 | 306 | 1946 | 868 |
| V／C Ratio（X） | 0.07 | 0.00 | 0.37 | 0.72 | 0.04 | 0.12 | 0.17 | 0.53 | 0.14 | 0.28 | 0.44 | 0.01 |
| Avail Cap（c＿a），veh／h | 363 | 0 | 490 | 385 | 620 | 526 | 402 | 1936 | 864 | 328 | 1946 | 868 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 49.3 | 0.0 | 52.2 | 41.2 | 38.0 | 38.6 | 12.3 | 17.5 | 13.4 | 13.4 | 16.2 | 12.3 |
| Incr Delay（d2），s／veh | 0.1 | 0.0 | 0.6 | 5.7 | 0.0 | 0.1 | 0.1 | 1.0 | 0.3 | 0.2 | 0.7 | 0.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.4 | 0.0 | 1.4 | 8.0 | 0.4 | 0.9 | 0.7 | 9.2 | 1.6 | 1.0 | 7.2 | 0.1 |

Unsig．Movement Delay，s／veh

| LnGrp Delay（d），s／veh | 49.3 | 0.0 | 52.8 | 46.9 | 38.0 | 38.6 | 12.3 | 18.5 | 13.7 | 13.6 | 17.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | D | A | D | D | D | D | B | B | B | B | B |
| Approach Vol，veh／h |  | 63 |  |  | 332 |  |  | 1209 |  | B |  |
| Approach Delay，s／veh | 52.0 |  |  | 45.5 |  |  | 17.8 |  | 957 |  |  |
| Approach LOS | D |  |  | D |  |  | B | 16.6 |  |  |  |


| Timer－Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Phs Duration（G＋Y＋Rc），s | 10.8 | 71.8 | 6.9 | 30.5 | 11.1 | 71.5 | 22.0 | 15.4 |
| Change Period（Y＋Rc），s | 6.4 | 6.1 | 5.0 | 5.6 | 6.4 | 6.1 | 5.0 | 5.6 |
| Max Green Setting（Gmax），s | 5.8 | 38.3 | 13.0 | 39.8 | 6.2 | 37.9 | 17.0 | 35.8 |
| Max Q Clear Time（g＿c＋I1），s | 3.8 | 19.4 | 2.9 | 4.3 | 4.6 | 24.3 | 18.9 | 5.4 |
| Green Ext Time（p＿c），s | 0.0 | 4.1 | 0.0 | 0.1 | 0.0 | 4.6 | 0.0 | 0.1 |

## Intersection Summary

| HCM 6th Ctrl Delay | 21.8 |
| :--- | ---: |
| HCM 6th LOS | C |

## Notes

User approved pedestrian interval to be less than phase max green．

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.8 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | A | A | $\mathbf{F}$ |  | M |  |
| Traffic Vol, veh/h | 48 | 63 | 50 | 1 | 0 | 18 |
| Future Vol, veh/h | 48 | 63 | 50 | 1 | 0 | 18 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 75 | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 52 | 68 | 54 | 1 | 0 | 20 |


| Major/Minor M | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 55 | 0 | - | 0 | 227 | 55 |
| Stage 1 | - | - | - | - | 55 | - |
| Stage 2 | - | - | - | - | 172 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1550 | - | - | - | 761 | 1012 |
| Stage 1 | - | - | - | - | 968 | - |
| Stage 2 | - | - | - | - | 858 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1550 | - | - | - | 735 | 1012 |
| Mov Cap-2 Maneuver | - | - | - | - | 735 | - |
| Stage 1 | - | - | - | - | 935 | - |
| Stage 2 | - | - | - | - | 858 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 3.2 |  | 0 |  | 8.6 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1550 | - | - | - | 1012 |
| HCM Lane V/C Ratio |  | 0.034 | - | - | - | 0.019 |
| HCM Control Delay (s) |  | 7.4 | - | - | - | 8.6 |
| HCM Lane LOS |  | A | - | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | - | 0.1 |

Assumptions and/or Givens
Elements of Design from AASHTO
Driver Eye Height
Truck
Object Height
Stopping Sight Distance
Passing Sight Distance
Vehicle Height
Driver Eye Location
From Edge of Major Rd Traveled Way Deceleration Rate (a)
Passenger Vehicle
Passenger Vehicle
Truck
Brake reaction time ( t )

AASHTO Re
$3.50 \mathrm{ft} \quad$ §3.2.6.1, p 3-15 $\begin{array}{ll}3.50 \mathrm{ft} \\ 7.60 \mathrm{ft} & \text { §3.2.6.1, p 3-15 } \\ \text { §3.2.6.1, p 3-15 }\end{array}$
$\begin{array}{ll}2.00 \mathrm{ft} & \S 3.2 .6 .2, \mathrm{p} 3-15 \\ 3.50 \mathrm{ft} & \S 3.2 .2 . \mathrm{p} 3.15\end{array}$
$3.50 \mathrm{ft} \quad \S 3.2 .6 .2, \mathrm{p} 3-15$
$14.50 \mathrm{ft} \quad$ §9.5.3.2.1, p 9-43
$11.20 \mathrm{ft} / \mathrm{sec}^{2} \quad$ §3.2.2.2, p 3-4
$\begin{array}{ll}\mathrm{N} / \mathrm{A} \mathrm{ft} \\ 2.50 \mathrm{sec} & \text { §3.2.2.1, } \mathrm{p} \mathrm{3-3}\end{array}$

Site Specific Data (Bike \& turn lanes are outside traveled way and are not considered) Major Street Design Speed ( $\mathrm{V}_{\text {maior }}$ )


Stopping Sight Distance $=$ Brake Reaction Distance + Braking Distance
Neglecting Effect of Grade

$$
\mathrm{d}=1.47 \mathrm{~V} \mathrm{t}+1.075 \frac{\mathrm{~V}^{2}}{\mathrm{a}}
$$

With Effect of Grade
Calculated d= 196.7

$$
\begin{array}{r}
\mathrm{d}=1.47 \mathrm{Vt}+\frac{\mathrm{V}^{2}}{30\left(\left(\frac{\mathrm{a}}{32.2}\right) \pm \mathrm{G}\right)} \\
\text { Calculated d}=\begin{array}{c}
196.3 \mathrm{ft}-\text { left } \\
200 \mathrm{ft}-\text { right } \\
196.3 \mathrm{ft}-\text { left } \\
200 \mathrm{ft}-\text { right }
\end{array}
\end{array}
$$

Page 1 of 4

| Design Vehicle | Time Gap ( $\mathrm{t}_{\mathrm{g}}$ ) |  |
| :---: | :---: | :---: |
| Passenger Car | 7.5 sec | Tbl 9-6, p 9-44 |
| Single-Unit Tuck | 9.5 sec | Tbl 9-6, p 9-44 |
| Combination Truck | 11.5 sec | Tbl 9-6, p 9-44 |
| Time gap adjustments |  |  |
| Add'l lanes to cross ( $1^{\text {st }}$ is assumed) |  |  |
| Passenger Car | 0.5 sec | See Notes |
| Trucks | 0.7 sec | below |
| Minor Approach Upgrade (Per each 1\%>3\%) | 0.2 sec | Tbl 9-5, p 9-37 |
| Site data |  |  |
| Major Road Lanes on Left Approach | 1.0 | §9.5.3.2.1, p 9-44 |
| Minor Road Approach Upgrade, if >3\% | 0 \% | §9.5.3.2.1, p 9-44 |

Time Gap based on site data
Design Vehicle Gap+Adj for Approach Grade>3\%+Adis for Add'I Lanes \& Median
Passenger Car
7.5 sec
9.5 sec
1.5

Single-Unit Tuck
Combination Truck

ISD to left \& right along Major Road ISD=1.47V $\mathrm{V}_{\text {maior }} \mathrm{t}_{9} \quad$ (fi)
Eq 9-1, p 9-45

|  |  | ISD to Left and Right |
| :---: | :---: | :---: |
| Passenger Car | calculated ISD= design ISD= | $\begin{array}{r} 330.8 \mathrm{ft} \\ 335 \mathrm{ft} \end{array}$ |
| Single-Unit Tuck | calculated ISD= design ISD= | $\begin{gathered} 419.0 \mathrm{ft} \\ 420 \mathrm{ft} \end{gathered}$ |
| Combination Truck | calculated ISD= design ISD= | $\begin{array}{r} 507.2 \mathrm{f} \\ 510 \mathrm{fl} \end{array}$ |

[^0]21-0480: Ashler Hills
Location: Access \& Ashler Hills

## Intersection Sight Distances (cont'd)

$\frac{\text { Case B2-Right Turn from the Minor Road }}{\&}$
AASHTO Ref
§9.5.3.2.2, p $9-47$
§9.5.3.2.3, p $9-48$

Case B3-Crossing Maneuver from the Minor Road

$$
\begin{array}{cc}
\text { Time Gap }\left(\mathrm{t}_{\mathrm{g}}\right) & \\
6.5 \mathrm{sec} & \text { Tbl 9-8, p 9-47 } \\
8.5 \mathrm{sec} & \& \\
10.5 \mathrm{sec} & \text { Tbl 9-10, p } 9-49
\end{array}
$$

Time gap adjustments
Add'l lanes to cross ( $1^{\text {st }}$ is assumed) - Case B-3 Only*
Passenger Car 0.5 sec 0.5 sec
0.7 sec
0.7 sec

Minor Approach Upgrade (Per each $1 \%>3 \%$ )
Case B-2 Only
0.1 sec
0.2 sec


Case B-3 Only
Site data
Major Road Lanes on Left Approach $\quad 1.0$ §9.5.3.2.2, p 9-4
Minor Road Approach Upgrade, if $>3 \%$
$0 \%$ §9.5.2.2 p9-4

Time Gap based on site data (sec)

| me Gap based on site data (sec) | B2 \& B3 B3 Only |
| :---: | :---: |
| Design Vehicle Gap+Adj for App | +Adjs for Add'l Lanes |
|  |  | Passenger Car

Single-Unit Tuck
$\begin{array}{rr}8.5 & 8.5 \\ 10.5 & 10.5\end{array}$
Combination Truck
$\mathrm{V}_{\text {majortg }}$ (ft)
Eq 9-1, p 9-45
ISD to left (B2/B3) \& right (B3) along Major Rd $\operatorname{lSD}=1.4 \mathrm{~V}_{\text {maiortg }}(\mathrm{f})$ )

| Passenger Car | $\begin{array}{r} \text { calculated ISD= } \\ \text { design ISD= } \end{array}$ | ISD to Left ISD to right (B2 \& B3) (B3 Only) |  |
| :---: | :---: | :---: | :---: |
|  |  | 286.7 | 286.7 |
|  |  | 290 | 290 |
| Single-Unit Tuck | calculated ISD= | 374.9 | 374.9 |
|  | design ISD= | 375 | 375 |
| Combination Truck | calculated ISD= | 463.1 | 463.1 |
|  | design ISD= | 465 | 465 |

*Number of major road lanes is irrelevant in Case B2.
The differences between Case B1 and Cases B2 \& B3 are reduced ime gaps and time gap adjustment for the minor approach upgrade.

21-0480: Ashler Hill
Location: Access \& Ashler Hills

## Intersection Sight Distances (cont'd

Case F-Left Turns from the Major Road
AASHTO Ref §9.5.3.6, p 9-56

| Design Vehicle | Time Gap $\left(\mathrm{t}_{\mathrm{g}}\right)$ |  |
| :--- | :---: | :---: |
| Passenger Car | 5.5 sec | Tb 9-16, p 9-57 |
| Single-Unit Tuck | 6.5 sec | Tbl 9-16, p9-57 |
| Combination Truck | 7.5 sec | Tbl 9-16, p 9-5 |

Time gap adjustments
Pa lanes to cross (1 assume
Passenger C
0.5 sec

See Notes to
Tb 9-16, p 9-57
Site data
Opposing Lanes (adj'd for x -wide median)
0.0

Time Gap based on site data
Design Vehicle Gap+Adj for Add'I Opposing Lanes Passenger Car
Single-Unit Tuck
5.5 sec
6.5 sec
6.5 sec
7.5 sec

ISD to front along Major Road

| Single-Unit Tuck | calculated ISD $=$ <br> design ISD | 286.7 ft <br> 290 ft |
| :--- | ---: | ---: |
| Combination Truck | calculated ISD= | 330.8 ft |

design ISD= $\quad 335 \mathrm{ft}$
The differences between Case F and Cases $\mathrm{B} 1, \mathrm{~B} 2$ \& B 3 are reduce ime gaps and no time gap adjustment for any minor approach upgrade
§9.5.3.6, p $9-58$

SIGHT DISTANCE SUMMARY

| Sight Distance Type | Governing <br> Case | Car | su Truck | Combo <br> Truck |
| :--- | :---: | ---: | ---: | ---: |
| Stopping |  |  |  |  |
| Without effect of grade |  | 200 | $\mathrm{~N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |
| With effect of grade on left |  | 200 | $\mathrm{~N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |
| With effect of grade on right |  | 200 | $\mathrm{~N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |
| Intersection | B 1 | 335 | 420 | 510 |
| To Right | B2/B3 | 290 | 375 | 465 |
| To Left | F | 245 | 290 | 335 |
| On Major Road |  |  |  |  |

Attachment H
March 2022


FIGURE 5.3-26 INTERSECTION \& DRIVEWAY DEPARTURE SIGHT DISTANCE REQUIREMENTS

## 1. Right-Angle Intersections

Right-angle intersections are those whose legs meet at an angle of 88 to 90 degrees. For these right-angle intersections the sight distances shown in Appendix 5-3A, Appendix 5-3B and Appendix 5-3C are to be used with Figure 5.3-26 to calculate the sight triangle. Appendices 5-3A and 5-3B present the intersection sight distances for all street classifications which were determined assuming passenger car traffic. Appendix 5-3C presents the sight distance requirements for varying roadway widths and design speeds for passenger cars, single unit trucks and combination trucks. If high volumes of truck traffic are anticipated, sight distances given in Appendix 5-3C will be used. Sight distances for vehicles turning left from the main street should also be considered and calculated based on the AASHTO Geometric Design of Highways and Streets.
2. Skewed Intersections

For skewed intersections where the intersection angles are less than 88 degrees, sight distances must be calculated in accordance with the procedures described in AASHTO's Geometric Design of Highways and Streets. Skewed intersection design must include appropriate design for pedestrian crossings and the location of curb ramps.
3. Intersections Within or Near a Curve

Sight distance measurements, identified as $S$ in Figure 5.3-26, need to follow the curved street alignment when the intersection is within or near a horizontal curve.
4. Traffic Safety Triangles

Traffic Safety Triangles should be used as a means to limit the height of structures, vegetation and other improvements on corner properties immediately adjacent to intersections. Safety triangles are not to be used as a substitute for intersection sight distance! Safety triangles provide additional visibility around corners for all intersection approaches and should be applied to the design of perimeter walls and
landscape features. Items within the safety triangle cannot be higher than 18 " measured from the roadway surface. Figure 5.3-27 depicts the method used to determine the safety triangle location. The sight distance requirements contained in both Figure 5.3-26 and Figure 5.3-27 are applied at all corner lots.
5. Right-of-Way at Corners

A minimum of 25 -foot radius rights-of-way shall be dedicated at street intersections to provide room for traffic control and sight distance.


| Major Street Classification | X (in feet) |
| :--- | :---: |
| Parkway, Expressway, Arterials, Major Collector | 25 |
| Minor Collector | 35 |
| * Local Streets | $35 / 60 / 70$ |

* If the standard right-of-way ( 46 ft . local residential, 60 ft . local collector) is not available, the safety triangle $(X)$ shall measure 60 ft . on local residential streets and 70 ft . on local collector streets from the centerlines of the streets.


## FIGURE 5.3-27 TRAFFIC SAFETY TRIANGLE ON CORNER PROPERTY

## E. Auxiliary Lanes

An exclusive turning lane permits separation of conflicting traffic movements and removes turning vehicles from the flow of through traffic. Figure 5.3-28 and Figure 5.3-29 depict the

Appendix 5-3C INTERSECTION \& DRIVEWAY SIGHT DISTANCE REQUIREMENTS

Six Lane Roadway

| Sight Distance (S) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Design <br> Speed | Passenger Car <br> (ft) |  | Single Unit <br> Truck (ft) |  | Combination <br> Truck (ft) |  |
|  | TH | LT | TH | LT | TH | LT |
| 25 | 350 | 350 | 470 | 455 | 540 | 530 |
| 30 | 420 | 420 | 560 | 545 | 650 | 635 |
| 35 | 490 | 490 | 655 | 635 | 760 | 740 |
| 40 | 560 | 560 | 780 | 725 | 865 | 845 |
| 45 | 630 | 630 | 840 | 815 | 975 | 950 |
| 50 | 700 | 700 | 935 | 905 | 1080 | 1055 |
| 55 | 770 | 770 | 1030 | 995 | 1190 | 1160 |

Four Lane Roadway

|  | Sight Distance (S) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Design <br> Speed | Passenger Car <br> (ft) | Single Unit <br> Truck (ft) |  | Combination <br> Truck (ft) |  |  |
|  | TH | LT | TH | LT | TH | LT |
| 25 | 315 | 335 | 415 | 430 | 490 | 500 |
| 30 | 375 | 400 | 500 | 515 | 590 | 600 |
| 35 | 440 | 465 | 585 | 600 | 685 | 700 |
| 40 | 500 | 530 | 665 | 685 | 785 | 800 |
| 45 | 565 | 565 | 750 | 770 | 880 | 900 |
| 50 | 625 | 665 | 835 | 855 | 980 | 1000 |
| 55 | 690 | 730 | 915 | 940 | 1075 | 1100 |

Three Lane Roadway

|  | Sight Distance (S) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Design <br> Speed | Passenger Car <br> (ft) |  | Single Unit <br> Truck (ft) |  | Combination <br> Truck (ft) |  |
|  | TH | LT | TH | LT | TH | LT |
| 25 | 260 | 295 | 340 | 375 | 415 | 450 |
| 30 | 310 | 355 | 410 | 450 | 495 | 540 |
| 35 | 360 | 415 | 475 | 525 | 580 | 630 |
| 40 | 415 | 470 | 545 | 600 | 660 | 720 |
| 45 | 465 | 530 | 610 | 675 | 745 | 810 |
| 50 | 515 | 590 | 680 | 750 | 825 | 900 |
| 55 | 570 | 650 | 745 | 825 | 910 | 990 |

Two Lane Roadway

|  | Sight Distance (S) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Design <br> Speed | Passenger Car <br> (ft) |  | Single Unit <br> Truck (ft) |  | Combination <br> Truck (ft) |  |
|  | TH | LT | TH | LT | TH | LT |
| 25 | 240 | 280 | 315 | 350 | 390 | 425 |
| 30 | 290 | 335 | 375 | 420 | 465 | 510 |
| 35 | 335 | 390 | 440 | 490 | 540 | 595 |
| 40 | 385 | 445 | 500 | 560 | 620 | 880 |
| 45 | 430 | 500 | 565 | 630 | 695 | 765 |
| 50 | 480 | 555 | 625 | 700 | 775 | 845 |
| 55 | 530 | 610 | 690 | 770 | 850 | 930 |

## Notes:

- TH=Through Movement, LT = Turn Movement
- Design speed by roadway classification is shown in Appendix 5-3A and Appendix 5-3B. Typically design speed is equal to the speed limit +10 mph.
- Refer to the 2004 AASHTO Geometric Design of Highways and Streets for additional information



[^0]:    CivTech

